

SPIN

MONITORING A
RESTLESS EARTH

<http://spin-itn.eu>

Coda waves, Surface Waves, Fiber Optics... Some challenges and results about the monitoring of concrete structures with ultrasonic waves

Odile Abraham



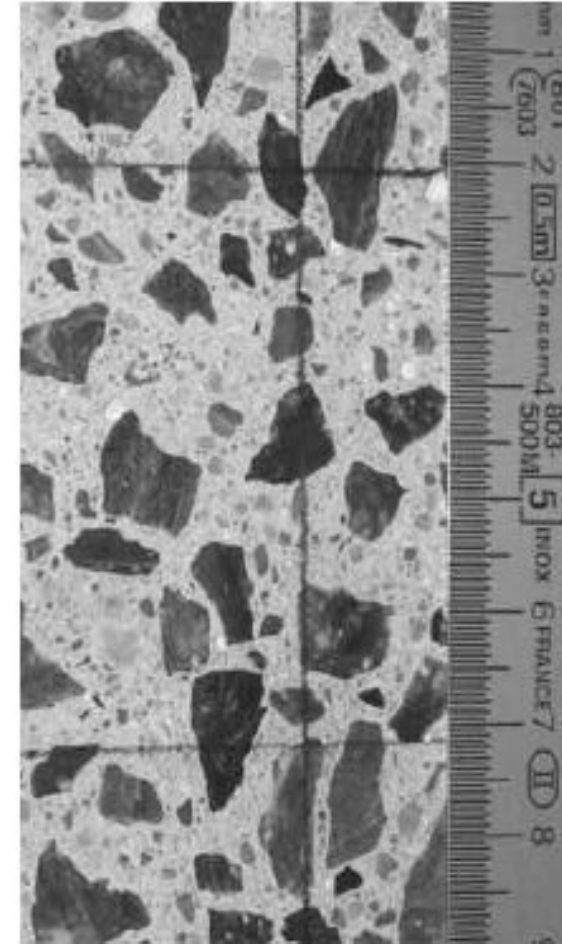
Université
Gustave
Eiffel

LABORATOIRE GEOEND
GÉOPHYSIQUE ET
ÉVALUATION NON
DESTRUCTIVE



Ludovic Bodet, Rabih Chammas, Mathieu Chekroun, Guangzhi Chen, Thibaud Devie, Olivier Durand, Jean-Baptiste Legland, Maximilien Lehujeur, Donatienne Leparoux, Vincent Métais, Pierric Mora, Shilin Qu, Géraldine Villain, Yuxiang Zhang, Jean-Paul Balayssac, Jean-François Chaix, Vincent Garnier, Benoit Hilloulin, Vincent Tournat, ...

Research has been “recently” focused on **reinforced concrete** with the aim to recover **quantitative information** on the **material properties**



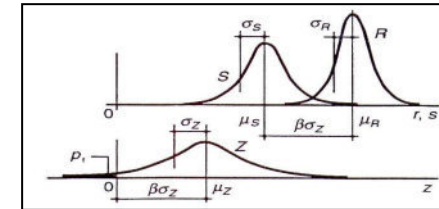
CONTEXT/France Non Destructive Testing (NDE) of concrete

NDE can be an alternative way for the assessment of concrete properties
→ **non intrusive and repeatable with reasonable cost**

Usual assessment of concrete properties
→ destructive testing on cores

Significant variability of concrete properties
→ the use of probabilistic models requires the assessment of this variability (cores \uparrow)

Most of the structures are very large
→ coring is prohibitive/impossible



But... Concrete properties have conjugated effects on NDEs

→ How to separate these effects?



French built heritage:

- 100000 important bridges
- 55 nuclear plants
- 350 electric dams
- Many buildings

Expected properties:

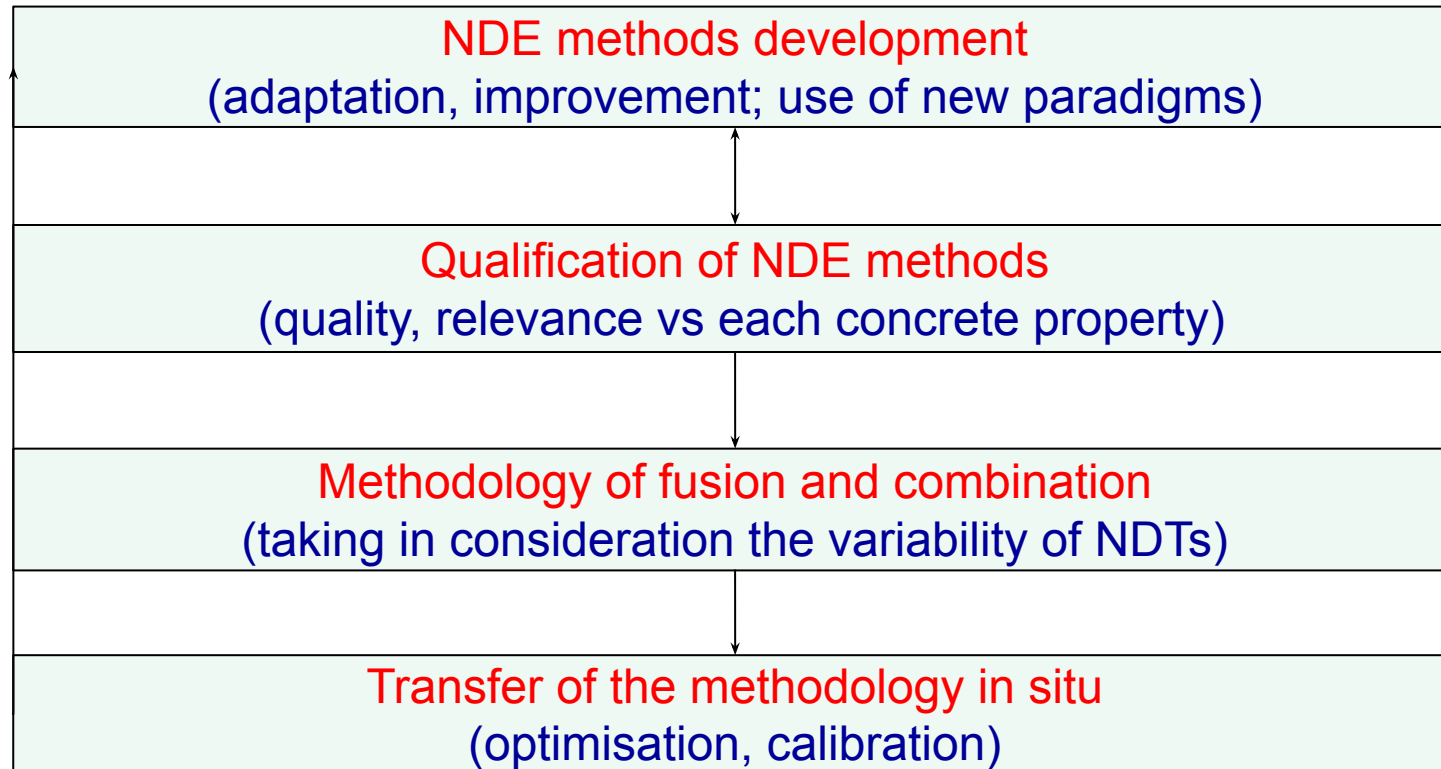
- E-modulus
- Porosity
- Moisture
- Chloride content
- Carbonation

- Thermal damage
- Stress

Several NDE methods are sensitive to these properties but the relationships between them are not direct

Both mean values and variability are necessary to assess

CONTEXT/France Non Destructive Testing (NDE) of concrete



NDE methods involved

surface



radar



capacitive



resistivity



permeability



surface wave dry
coupling



surface wave
air coupling



diffuse wave
DAET, ATME



TREND

NDE methods involved

surface



radar



capacitive



resistivity



permeability



surface wave dry coupling



surface wave air coupling



diffuse wave
DAET, ATME



TREND

volume



ultrasonic transmission



ultrasonic pulse echo



impact echo



(Nonlinear) coda wave interferometry

acoustics

NDE methods involved

surface



radar



capacitive



resistivity



permeability



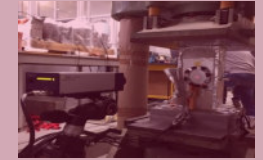
surface wave dry coupling



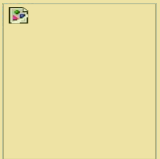
surface wave air coupling



diffuse wave
DAET, ATME



TREND



ultrasonic transmission



ultrasonic pulse echo



impact echo



(Nonlinear) coda wave interferometry

volume

acoustics

Low TRL

Outline

- **Recovering some concrete material properties**
 - fusion
- **Focus on Surface Waves (NDE/SHM)**
 - cover concrete
 - increasing TRL
- **Focus on Coda Waves**
 - monitoring
 - non linear
- **Fibers Optics at ultrasonics frequency**
 - project startings

Recovering some concrete material properties

Laboratory benchmarks are designed for controlling concrete properties



Involved properties: moisture, porosity, E-modulus, carbonation, chlorides, thermal damage, stress



Concrete slab size:
50 cm x 25 cm x 12 cm

Recovering some concrete material properties

All the NDE measurements are performed at the same time



Measurement processing and extraction of **observables/features** (velocity, attenuation, resistivity, etc)

L1 = UPE (UPE) + B (S) + Radar (C) + UPE (S) + OS (S) + Resist (C)
 L2 = LMA (OS, CL, CT, ARL)
 L3 = ECL (OS)
 L4 = Resis
 L5 = Resistive

Date	THERMIQUE											
	Etat 2 (300 °C)		Etat 2 (150 °C)		Etat 2 (1200 °C)		Etat 2 (2000 °C)		Etat 2 (2000 °C)		Etat 2 (2000 °C)	
	Face A	Face B	Face A	Face B	Face A	Face B	Face A	Face B	Face A	Face B	Face A	Face B
JOUR 1 : Samedi 30 mars	Preparation, Installation											
09h-09h												
10h-10h												
11h-11h												
12h-12h												
13h-13h												
14h-14h												
15h-15h												
16h-16h												
17h-17h												
18h-18h												
JOUR 2 : Mardi 31 mars												
09h-09h												
10h-10h												
11h-11h												
12h-12h												
13h-13h												
14h-14h												
15h-15h												
16h-16h												
17h-17h												
18h-18h												
JOUR 3 : Mercredi 1 avril												
09h-09h												
10h-10h												
11h-11h												
12h-12h												
13h-13h												
14h-14h												
15h-15h												
16h-16h												
17h-17h												
18h-18h												
JOUR 4 : Jeudi 2 avril												
09h-09h												
10h-10h												
11h-11h												
12h-12h												
13h-13h												
14h-14h												
15h-15h												
16h-16h												
17h-17h												
18h-18h												
JOUR 5 : Vendredi 3 avril												
09h-09h												
10h-10h												
11h-11h												
12h-12h												
13h-13h												
14h-14h												
15h-15h												
16h-16h												
17h-17h												
18h-18h												

Recovering some concrete material properties

Variance of NDE observables is quantified at different scales

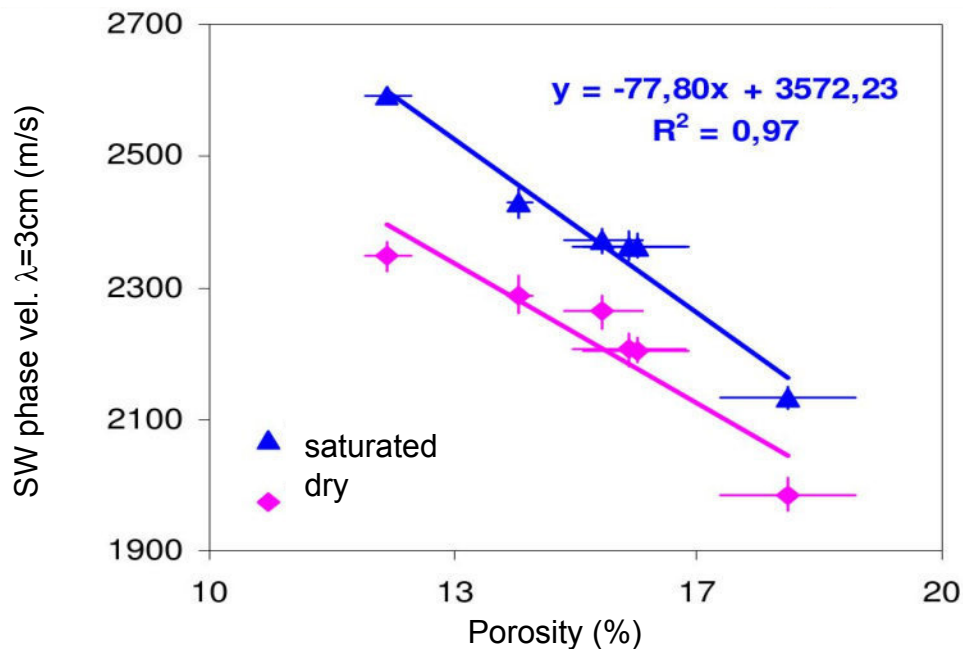


- Repeatability: V1
- In a same homogeneous sample: V2
- In a same batch: V3
- Between different concretes: V4

NDE observables/features vs concrete properties

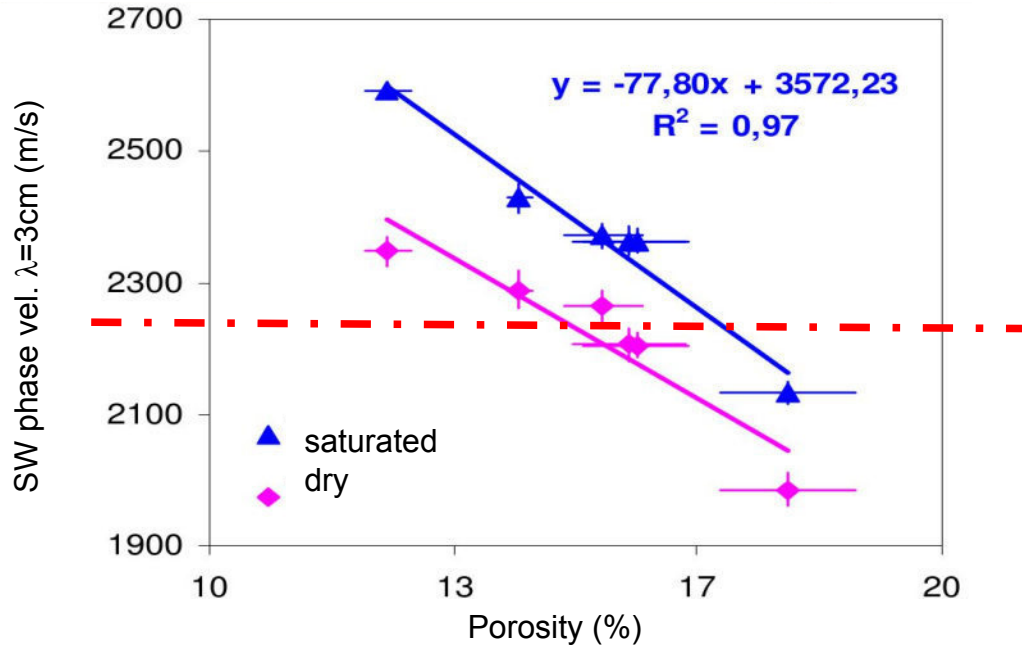
But... Concrete properties have conjugated effects on NDTs

→ **How to separate these effects?**



NDE observables/features vs concrete properties

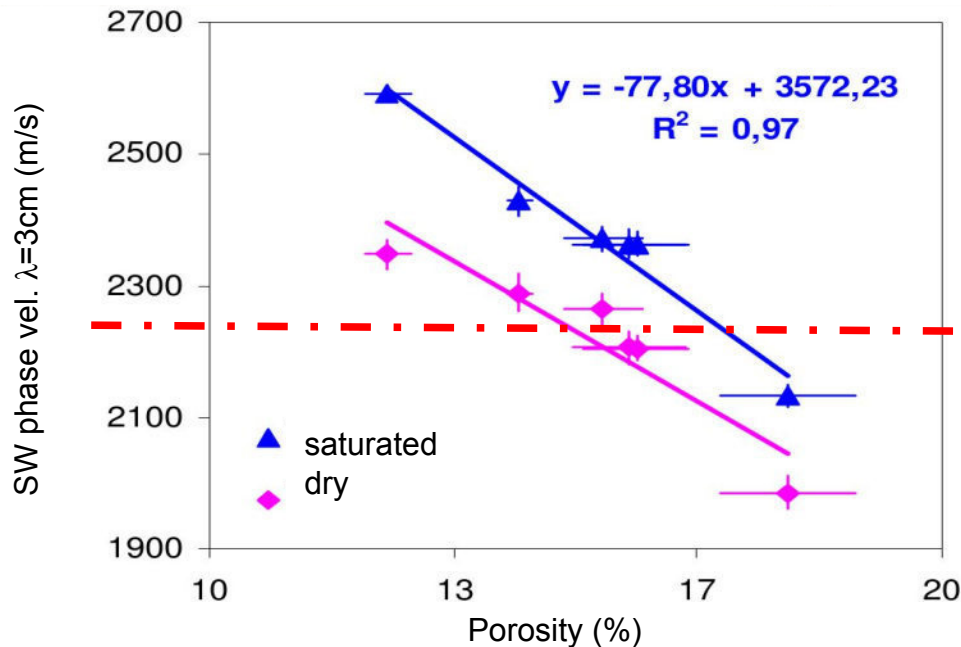
But... Concrete properties have conjugated effects on NDTs
→ **How to separate these effects?**



NDE observables/features vs concrete properties

But... Concrete properties have conjugated effects on NDTs

→ **How to separate these effects?**



Linear regression models between NDT observables (Obs) and two concrete properties (cp_1 and cp_2)

$$Obs = A. cp_1 + B. cp_2 + C$$

NDE observables/features vs concrete properties

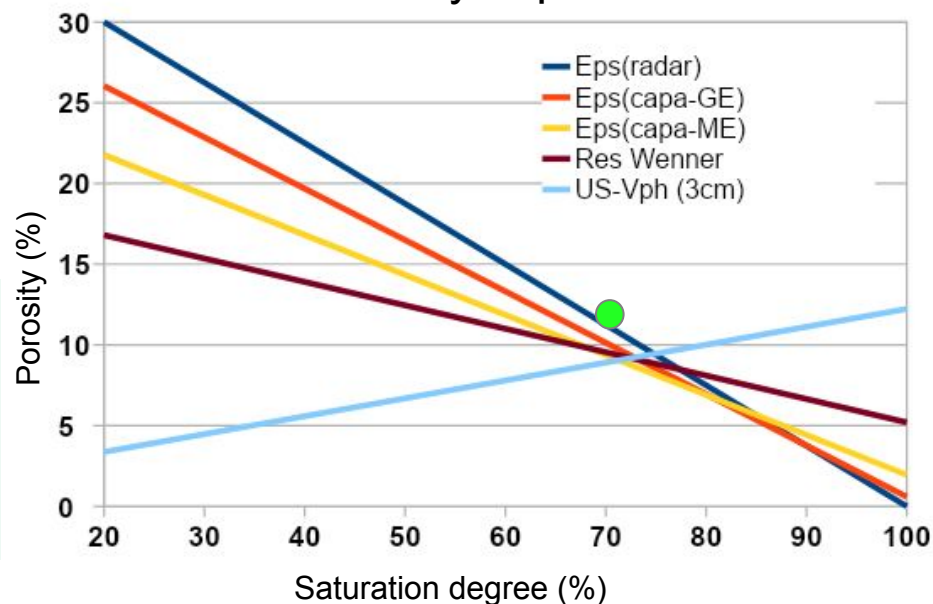
But... Concrete properties have conjugated effects on NDTs

→ **How to separate these effects?**

Combination of techniques

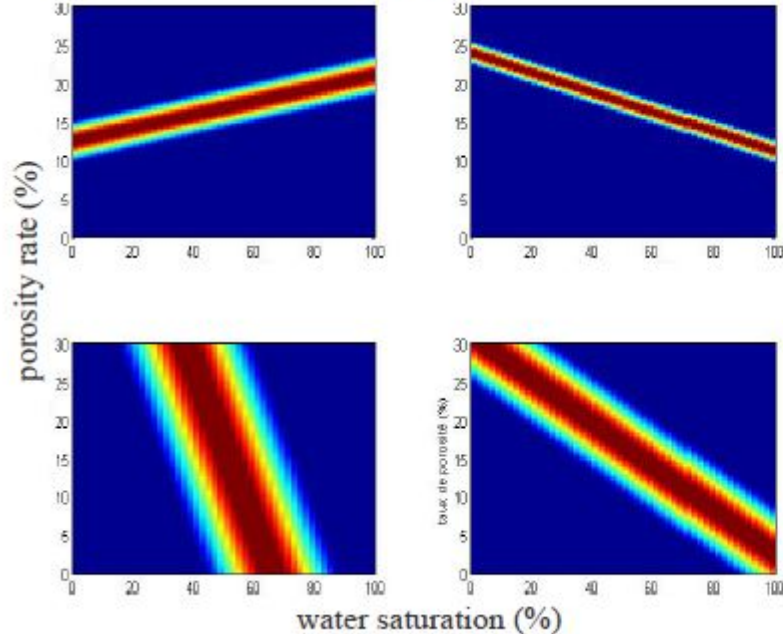
- Which methods?
- How to combine them?
- With which confidence?
- How to transfer on site this methodology ?

laboratory experiments



NDE observables/features vs concrete properties

Distributions provided by each measurement



General aim (data fusion):

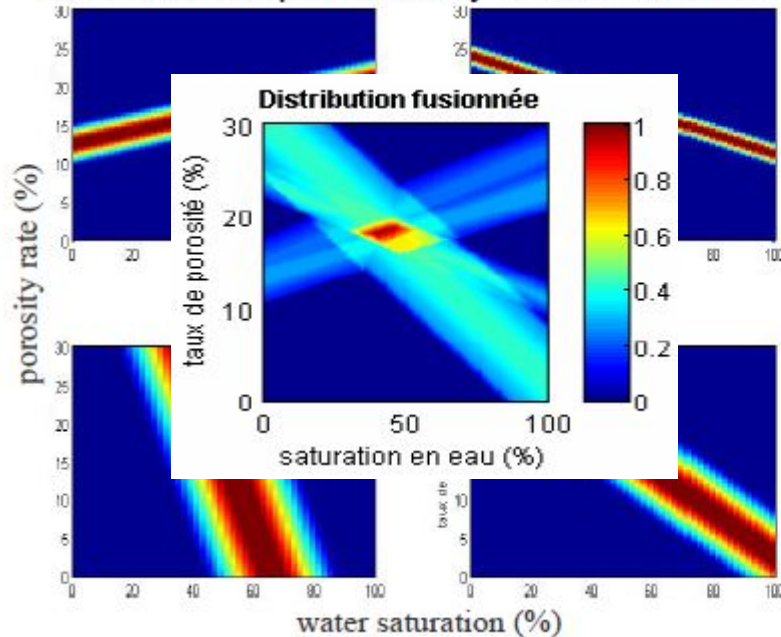
- to collect and combine information from different sources to provide more precise and reliable information
- to deal with uncertain and imprecise data

Distribution of possibilities is linked to the quality and relevance of the measurements

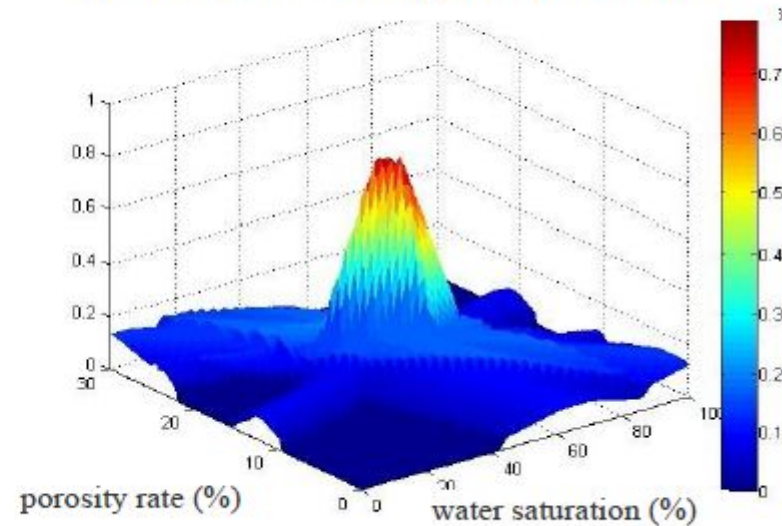
$$Obs = A \cdot cp_1 + B \cdot cp_2 + C$$

NDE observables/features vs concrete properties

Distributions provided by each measurement



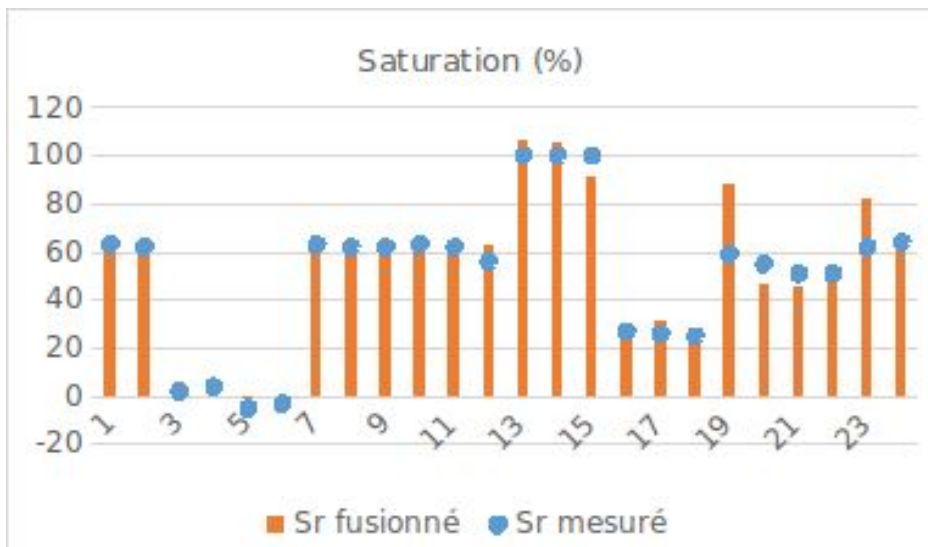
Distribution resulting from data fusion



$$Obs = A. cp_1 + B. cp_2 + C$$

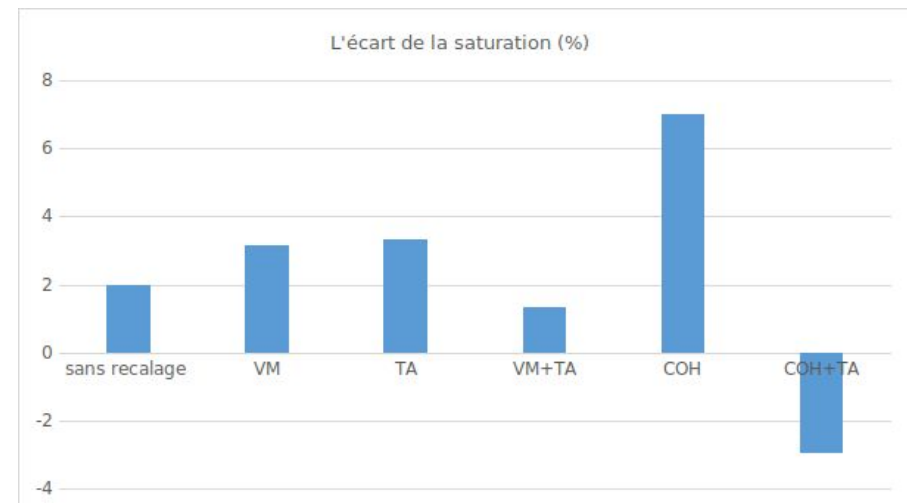
Distribution of possibilities is linked to the quality and relevance of the measurements

NDE observables/features vs concrete properties

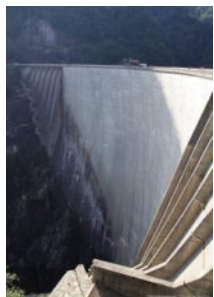


General aim (data fusion):

- to collect and combine information from different sources to provide more precise and reliable information
- to deal with uncertain and imprecise data

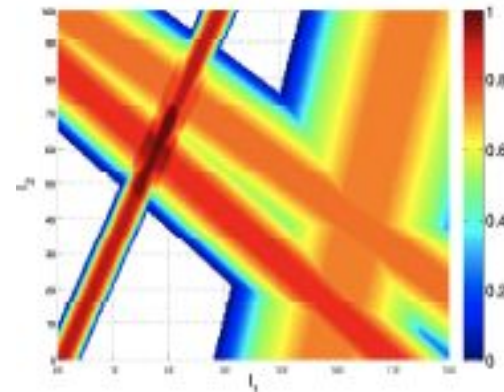


NDE observables/features vs concrete properties

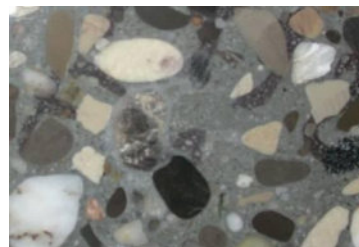


Chemistry

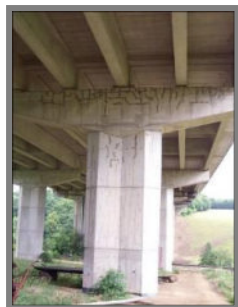
Mechanics



Composition

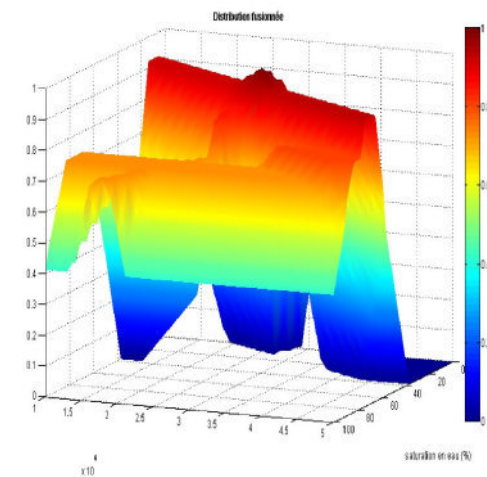


Environment



History

Need corrections and adjustments to adapt in the context of on site NDT



NDE observables/features vs concrete properties



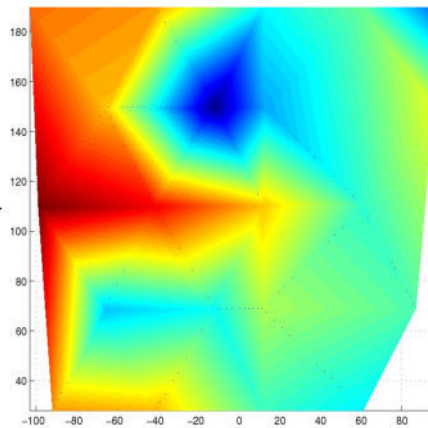
**Non-destructive Testing
and Evaluation of
Civil Engineering Structures**

Edited by
Jean-Paul Balayssac and Vincent Garnier

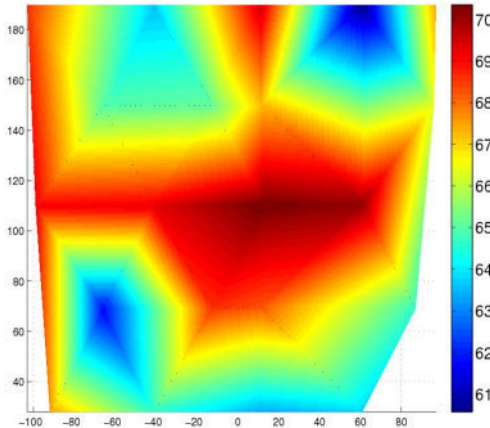
ISTE
PRESS



Methods:
US Velocity – Capacity
Impact Echo – Radar



Degree of saturation (%)



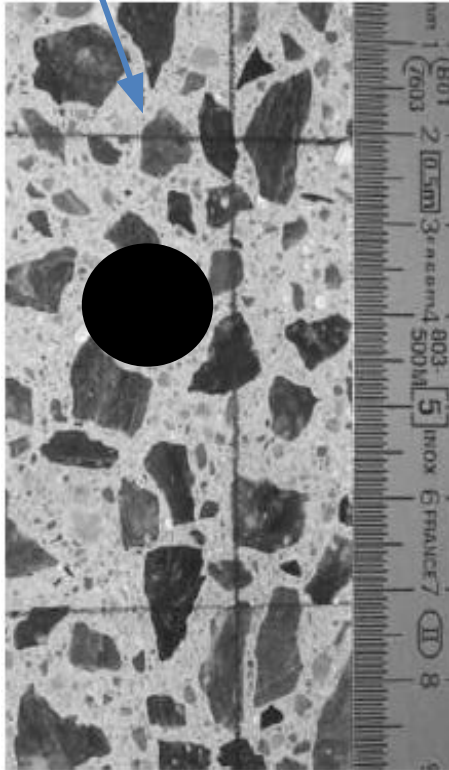
Compressive strength (MPa)

Outline

- **Recovering some concrete material properties**
 - fusion
- **Focus on Surface Waves (NDE/SHM)**
 - cover concrete
 - increasing TRL
- **Focus on Coda Waves**
 - monitoring
 - non linear
- **Fibers Optics at ultrasonics frequency**
 - project startings

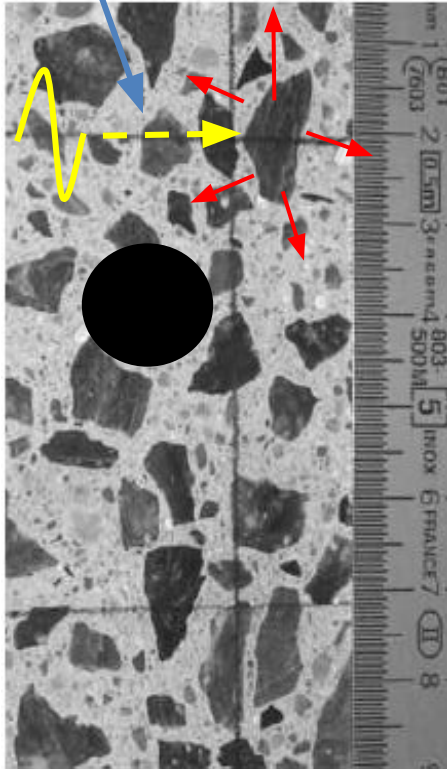
Focus on ultrasonic Surface Waves

CONTEXT: Cover concrete



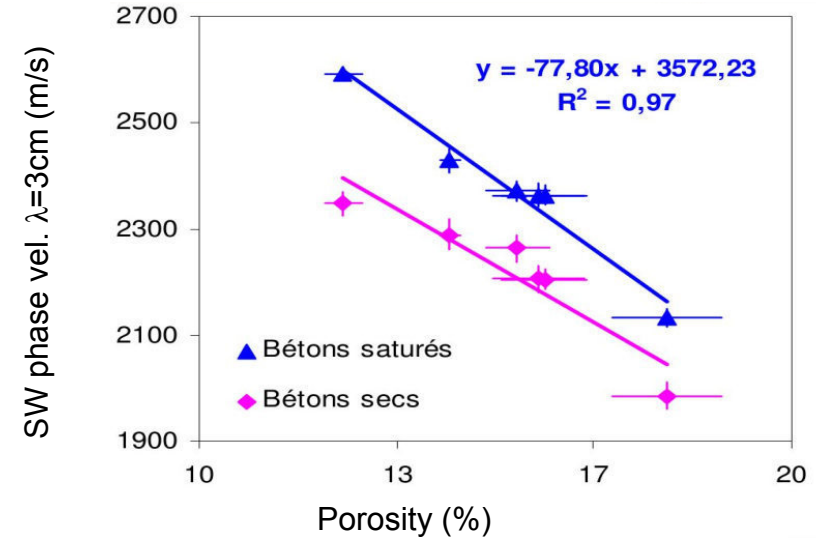
Focus on ultrasonic Surface Waves

CONTEXT: Cover concrete



Investigation depth:
~3–5 cm
Depth resolution:
0,5 – 1 cm
Largest aggregate size:
~2–3 cm

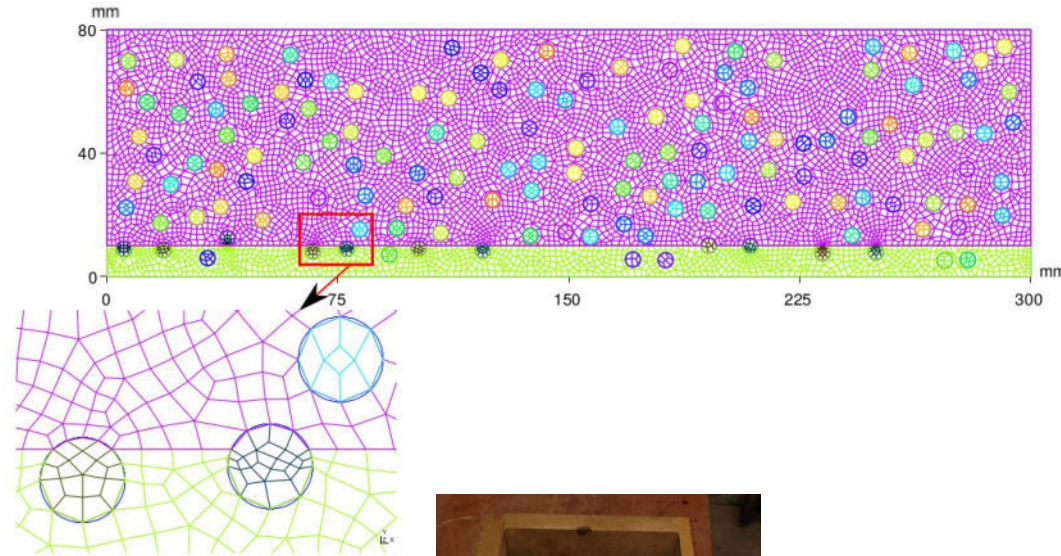
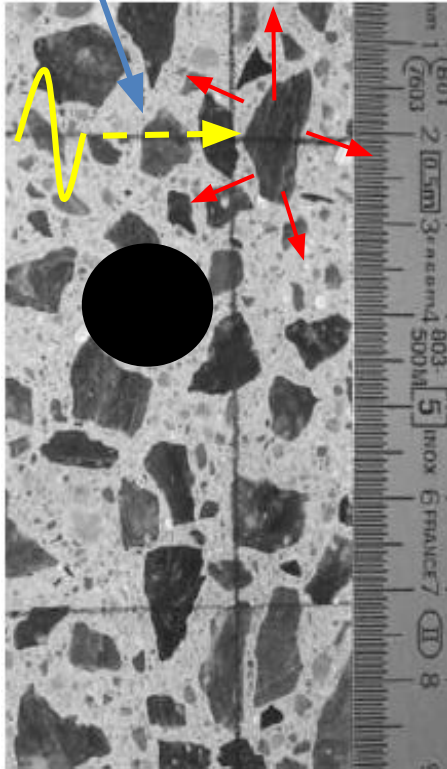
Can scattering be neglected ?



AIM: reach a precision of "0,5" on the estimated concrete porosity (expressed in %) thanks to SW phase velocity

Focus on ultrasonic Surface Waves

CONTEXT: Cover concrete

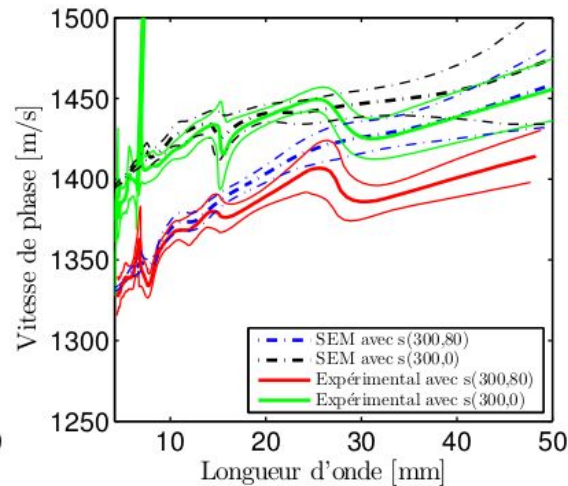
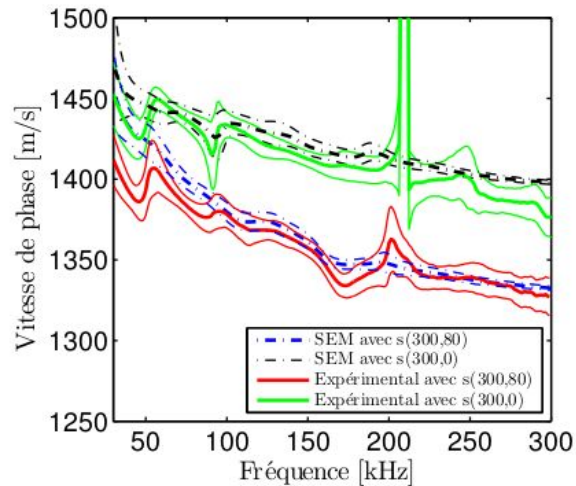
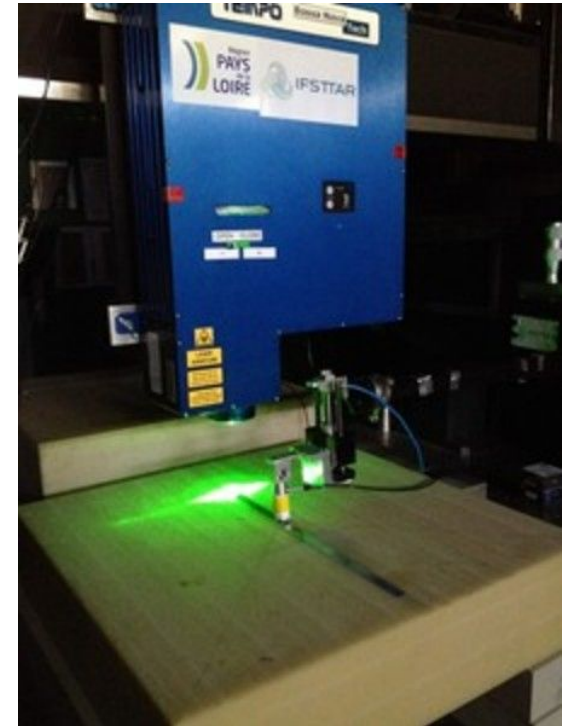
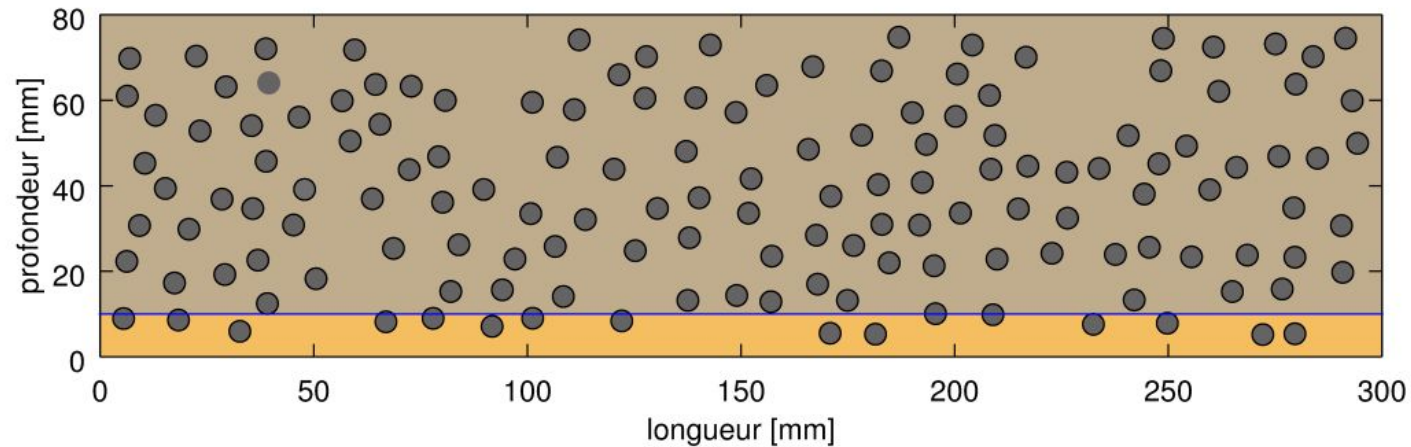


SEM2D
Y. Capdeville



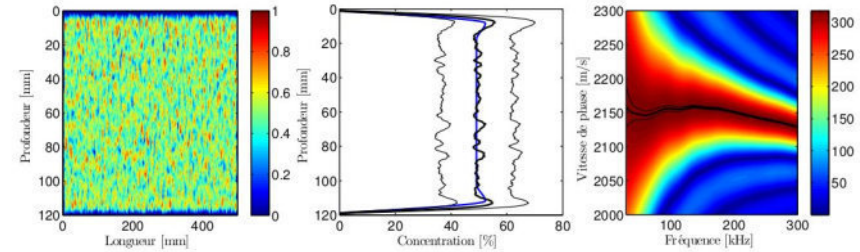
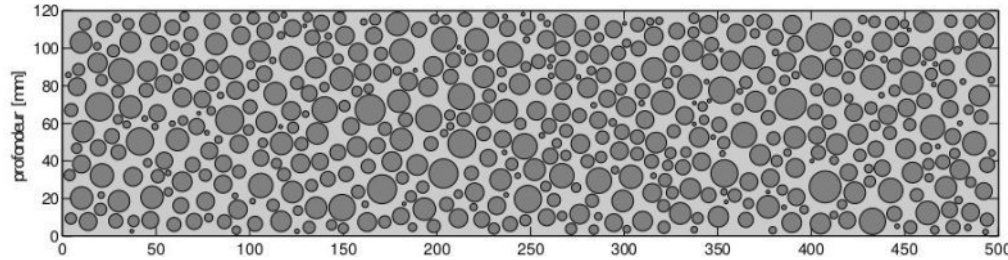
Can we use for each layer homogenized properties to compute the phase velocity dispersion curve ?

Focus on ultrasonic Surface Waves



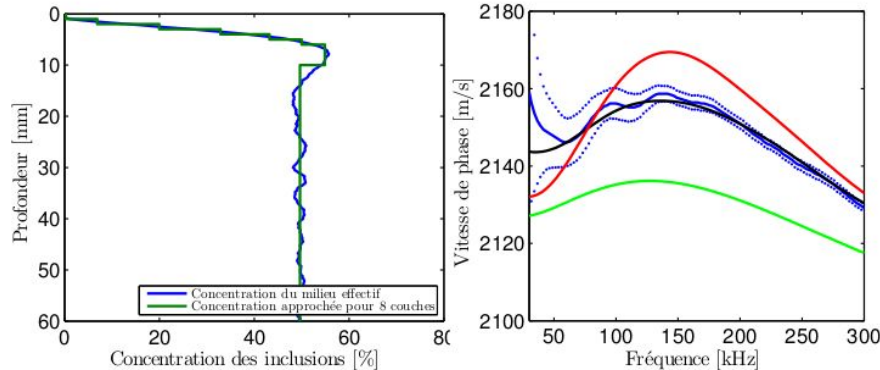
Coherent SW phase velocity dispersion curve requires more than 20 disorders (for a concentration of 12%)

Focus on ultrasonic Surface Waves



← 17 disorders

8 layers



Inversion results (Geopsy, Dinver, Conoir & Norris (2010))



SEM2D

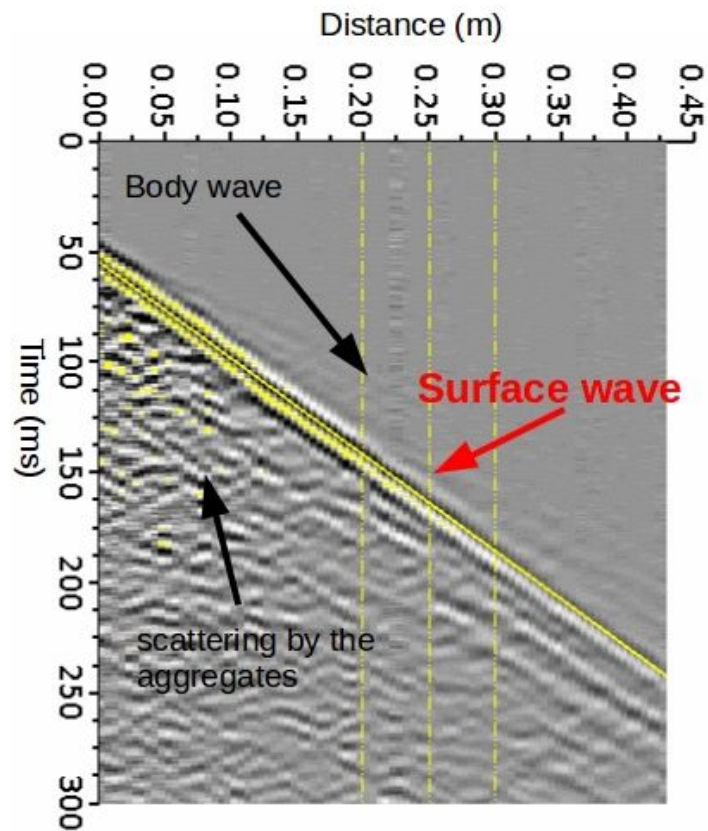
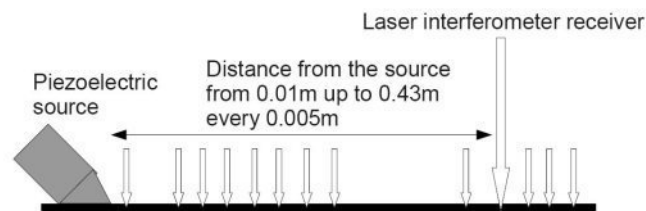
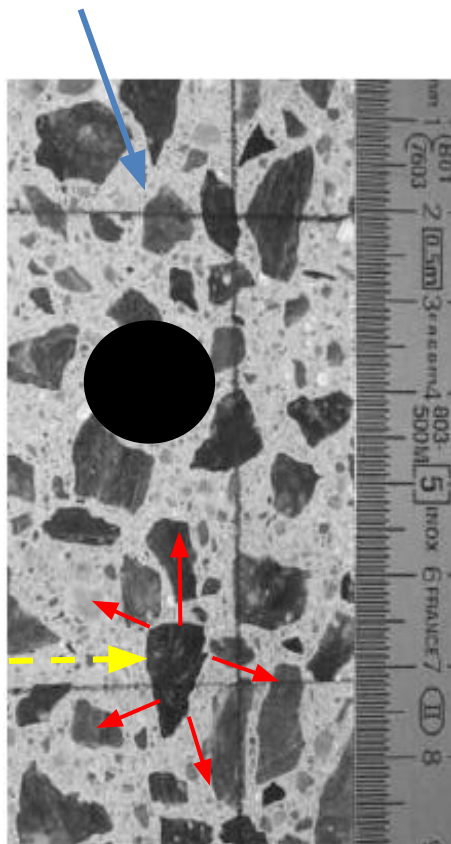
Conoir & Norris (2010)

ISA

Christensen & Lo (1079)

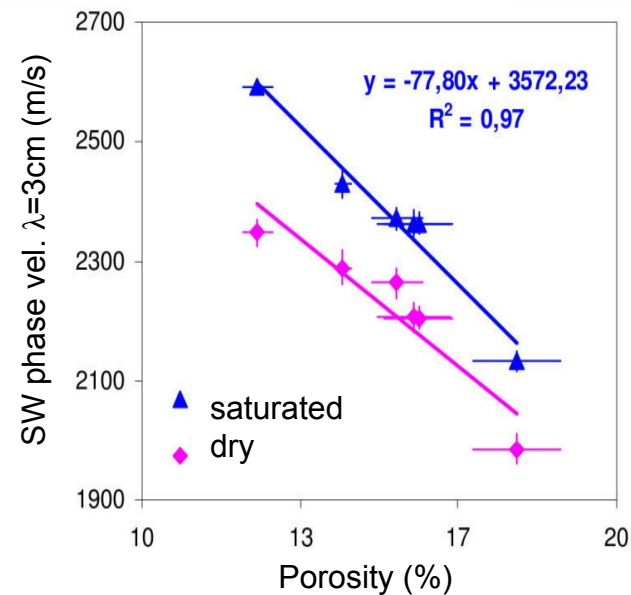
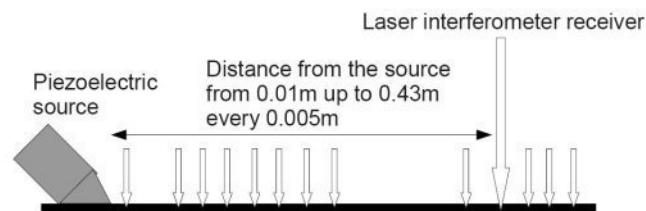
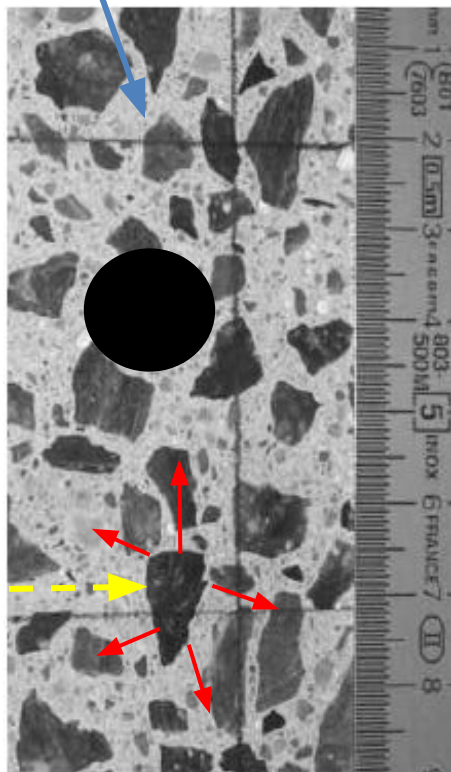
Focus on ultrasonic Surface Waves

CONTEXT: Cover concrete

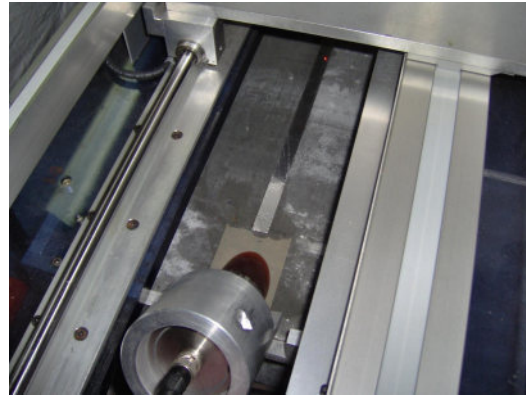


Focus on ultrasonic Surface Waves

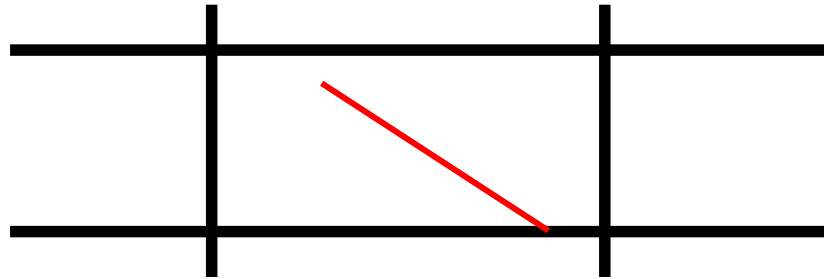
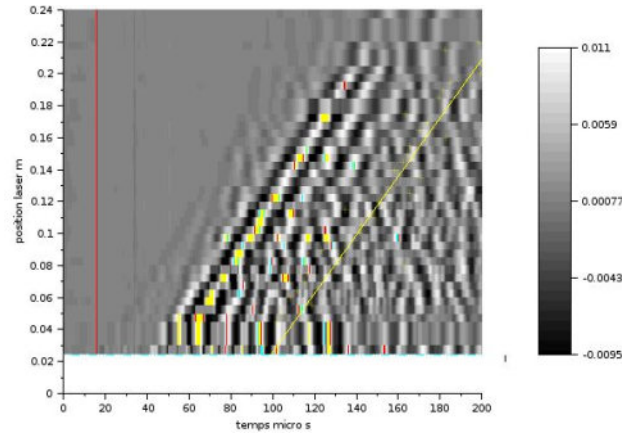
CONTEXT: Cover concrete



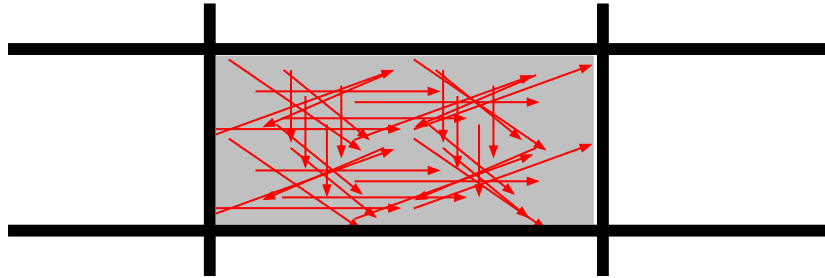
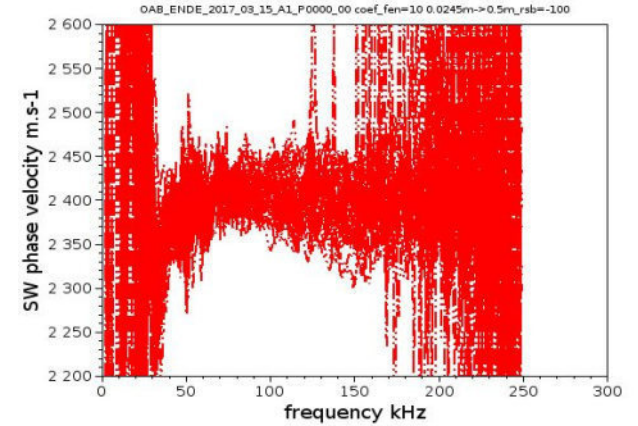
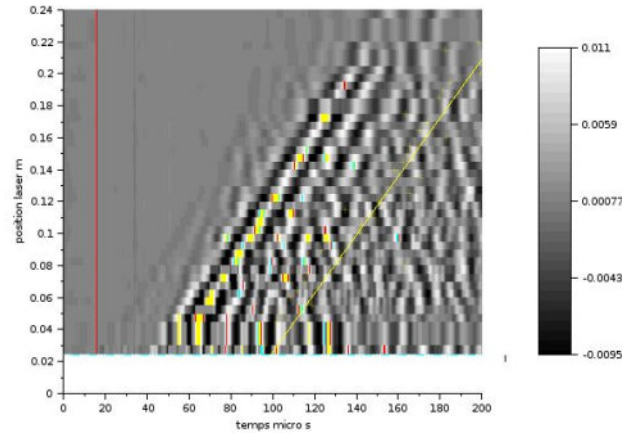
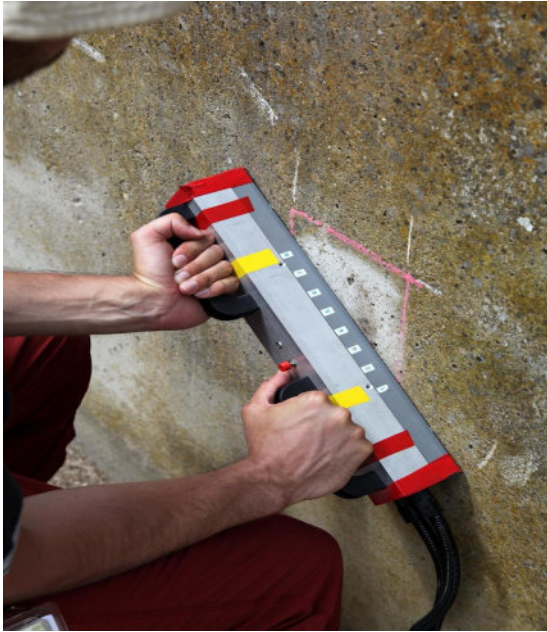
Focus on ultrasonic Surface Waves



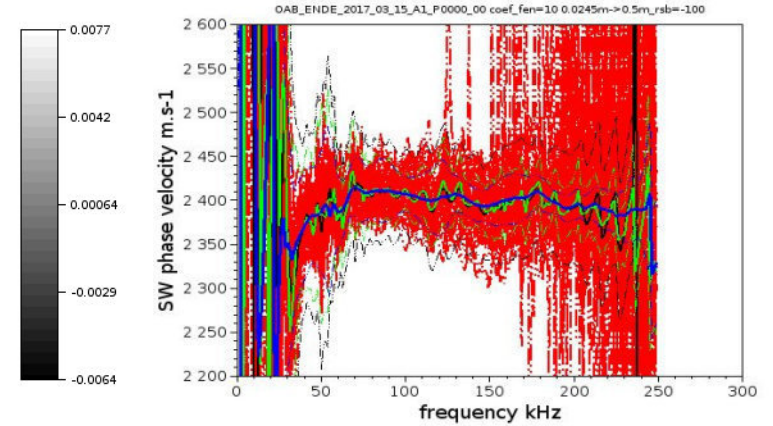
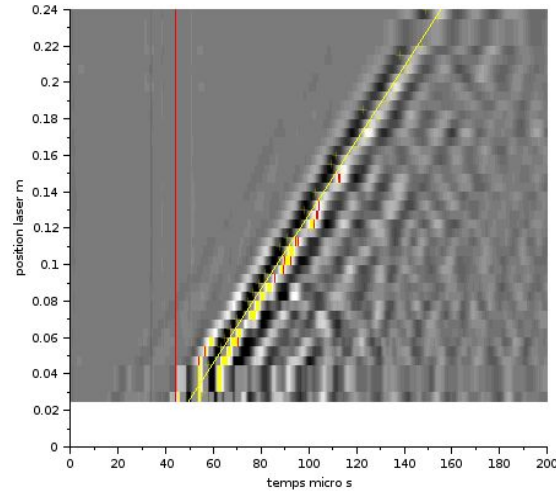
Focus on ultrasonic Surface Waves



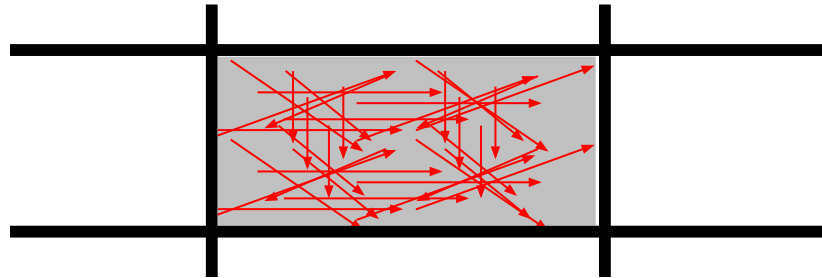
Focus on ultrasonic Surface Waves



Focus on ultrasonic Surface Waves



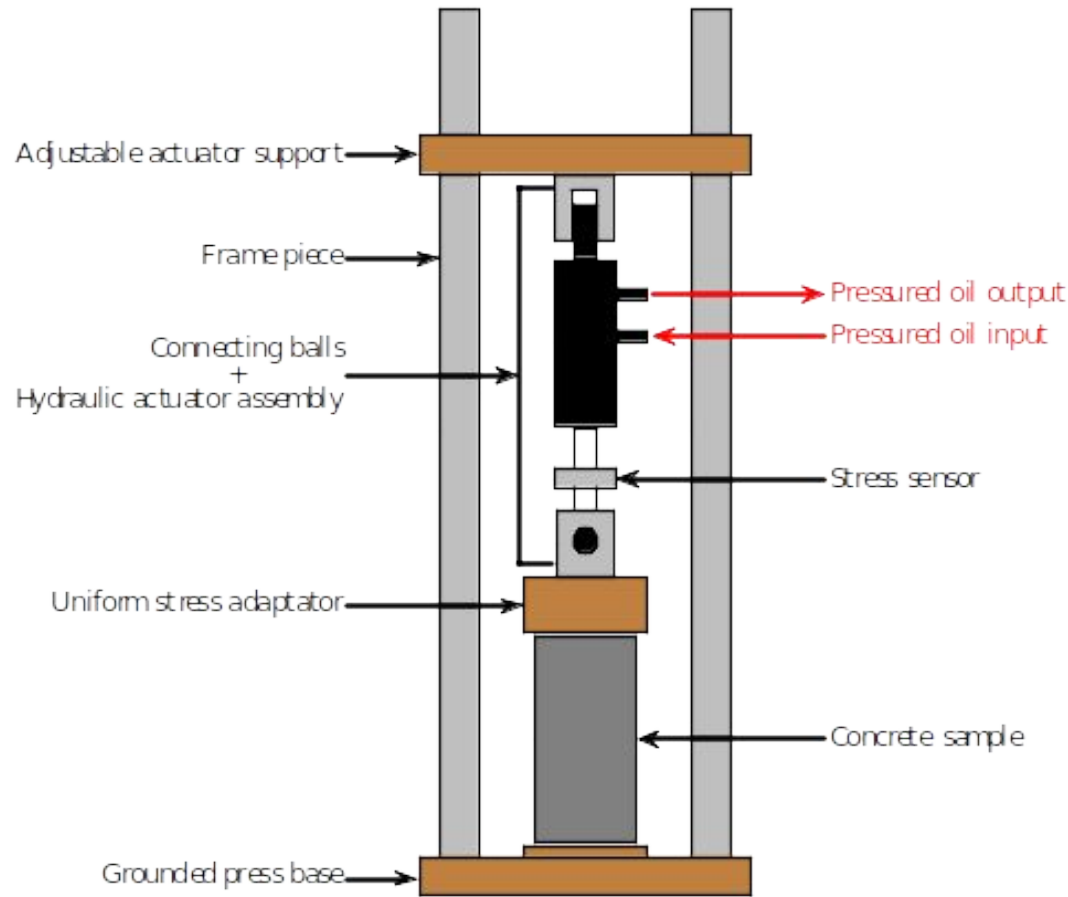
- $V\phi$ of individual seismograms
- Average of individual dispersion curve $V\phi$
- $V\phi$ of average seismograms
- $V\phi$ of average seismograms windowed



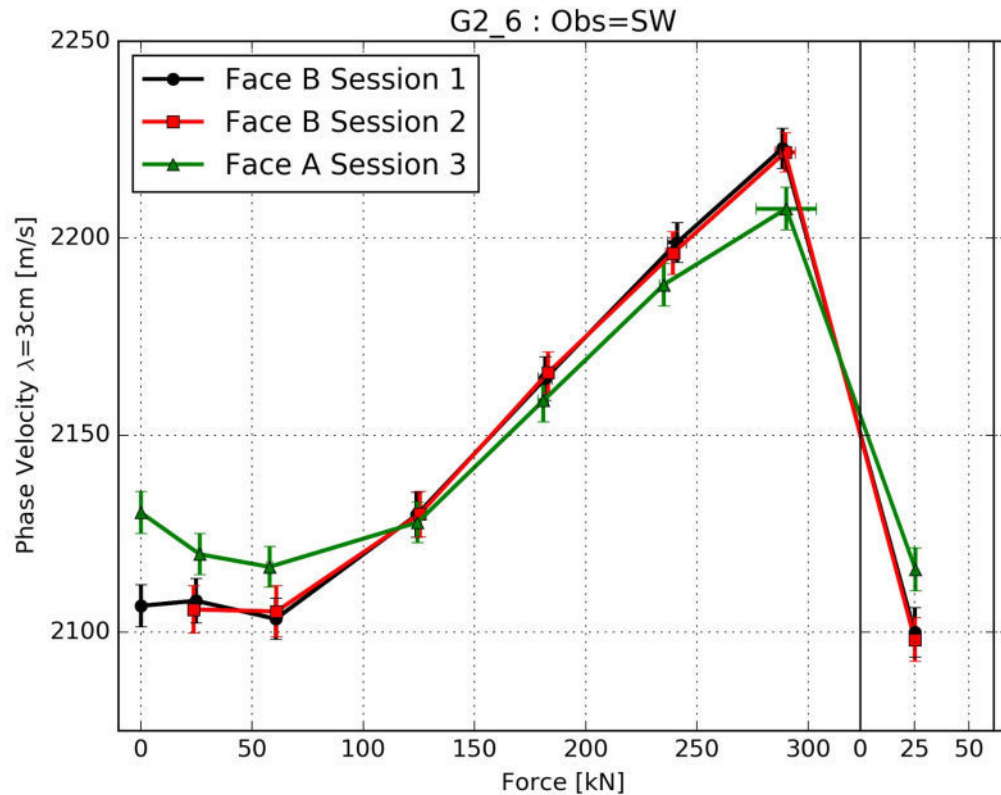
Coherent field



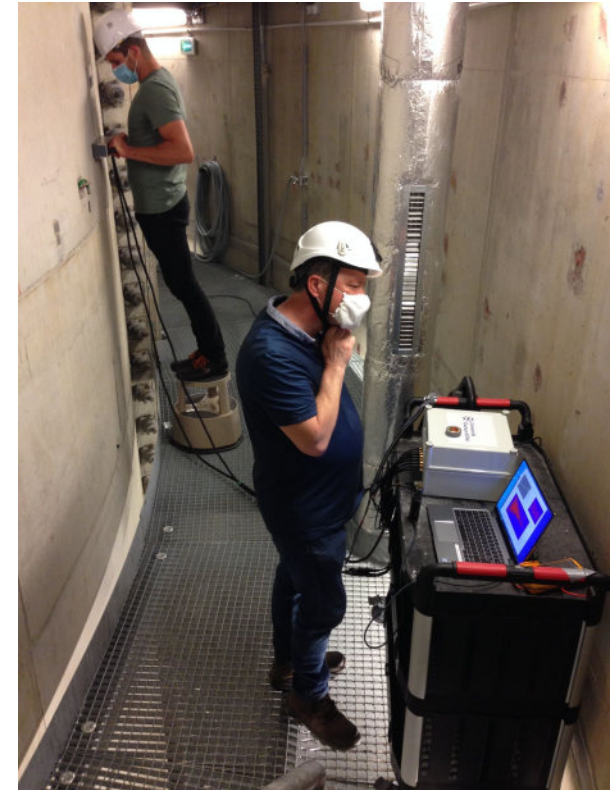
Focus on ultrasonic Surface Waves



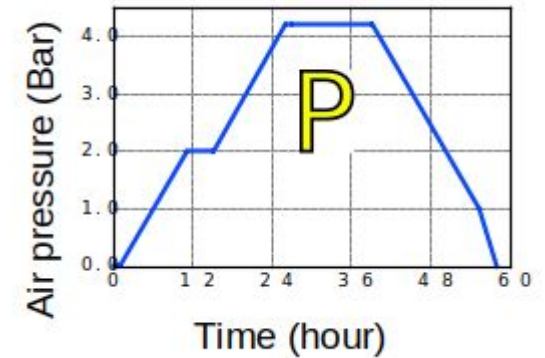
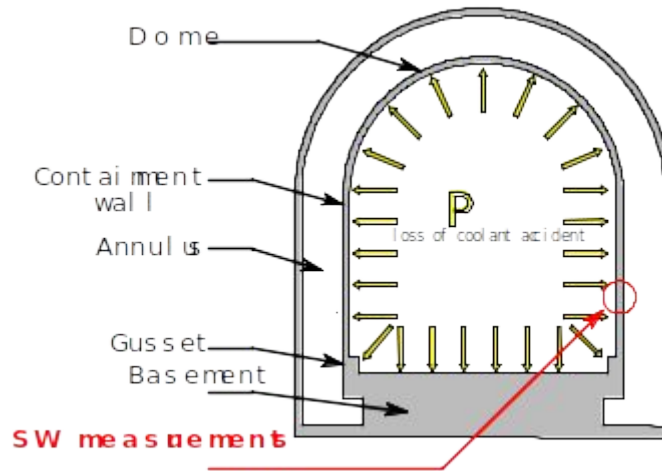
Focus on ultrasonic Surface Waves



Focus on ultrasonic Surface Waves



Focus on ultrasonic Surface Waves

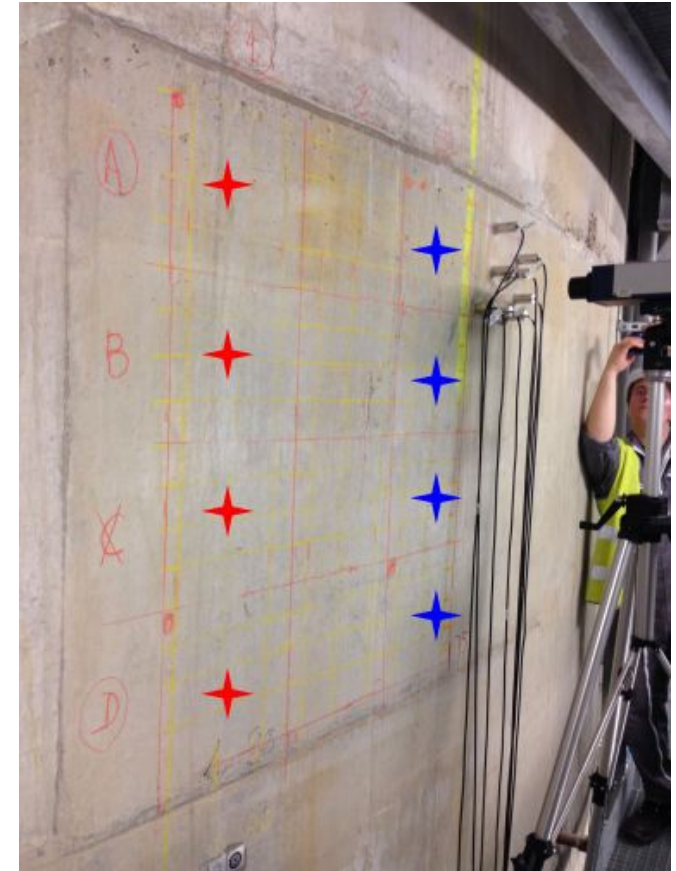
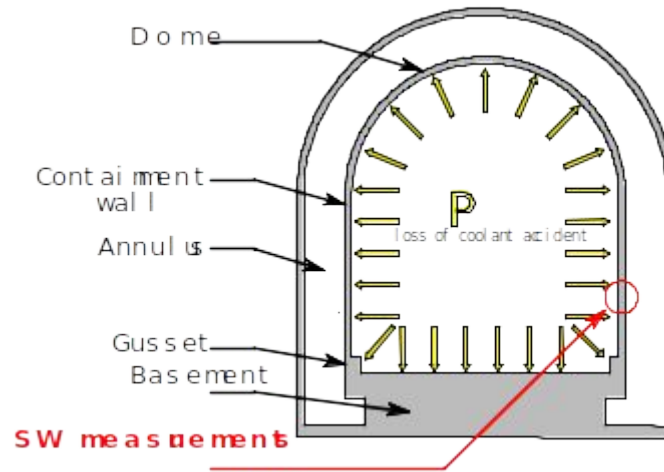


1 bar =
0.1 MPa =
14.5 psi

Nuclear containment plant

- 30 m height
- 5000 t of concrete
- 700 sensors
- 2 km of fiber optic

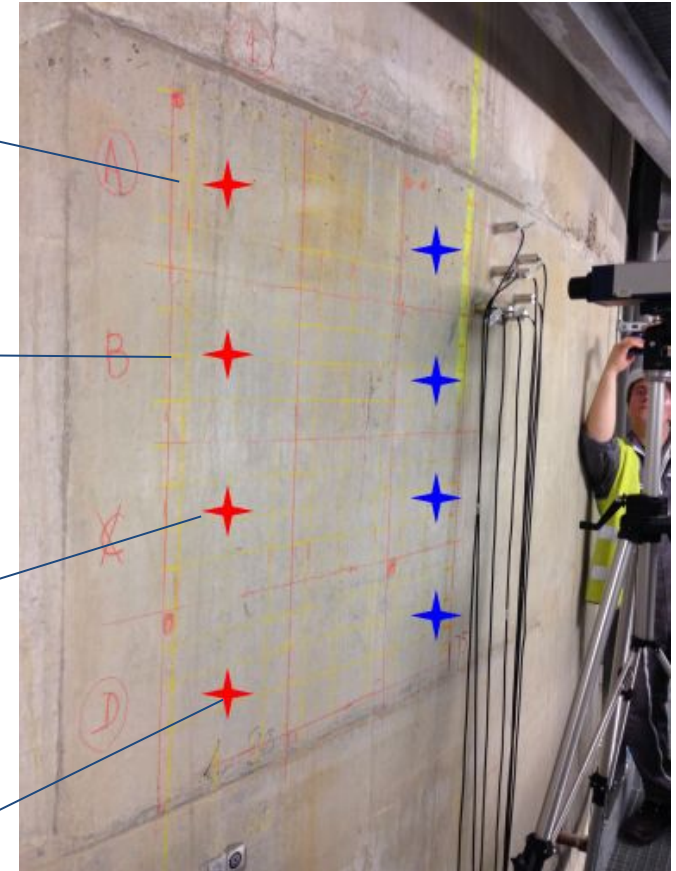
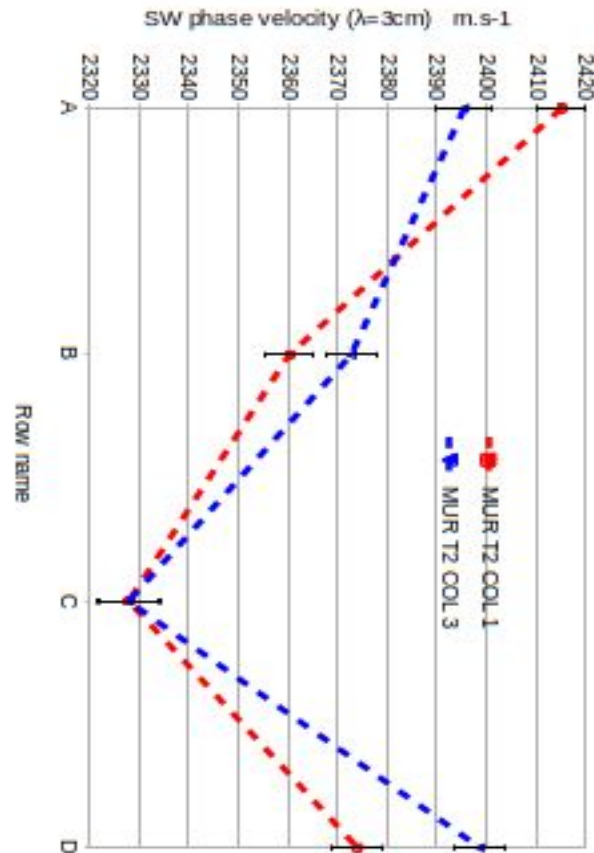
Focus on ultrasonic Surface Waves



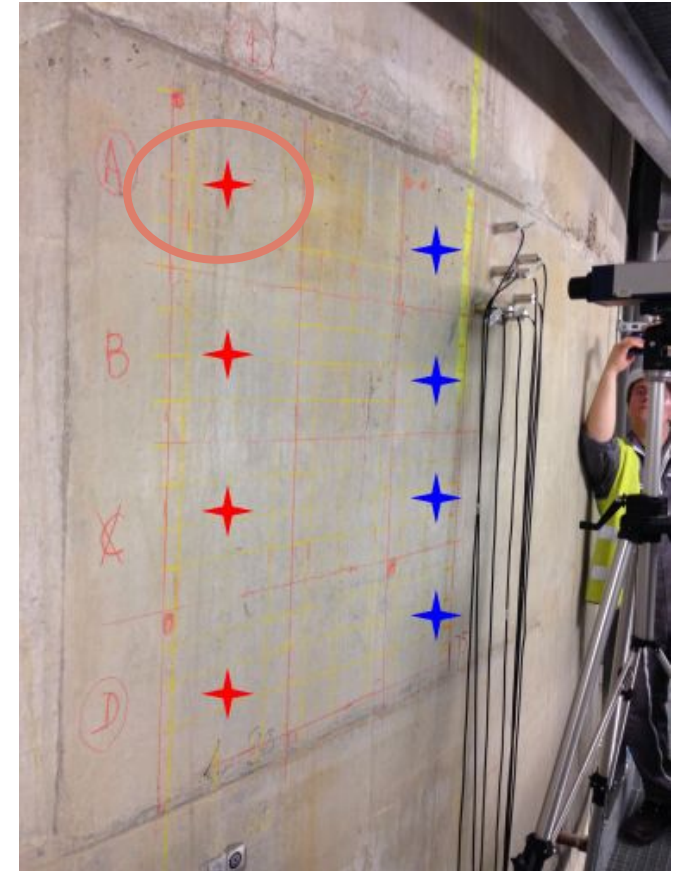
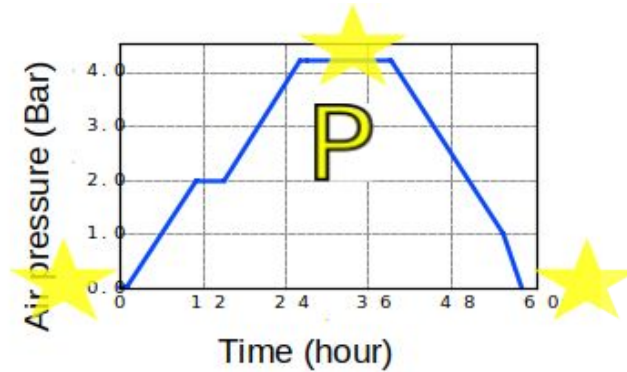
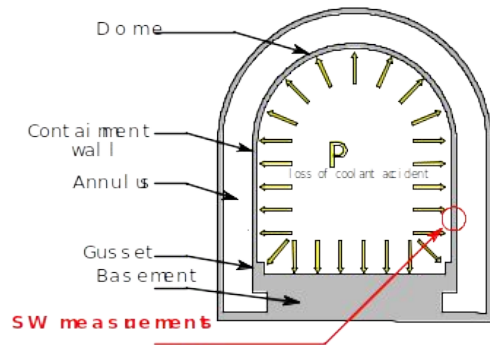
Nuclear containment plant

- 30 m height
- 5000 t of concrete
- 700 sensors
- 2 km of fiber optic

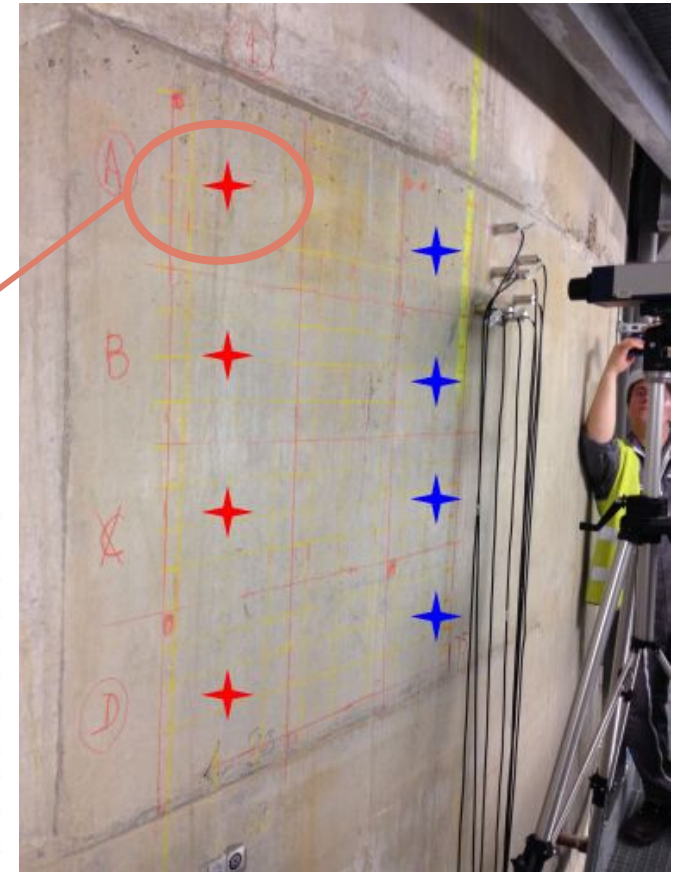
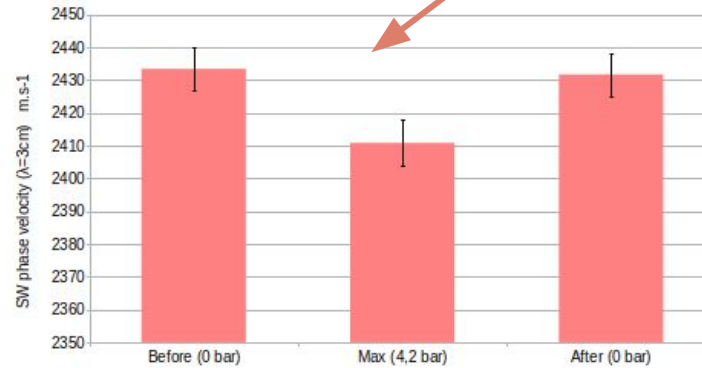
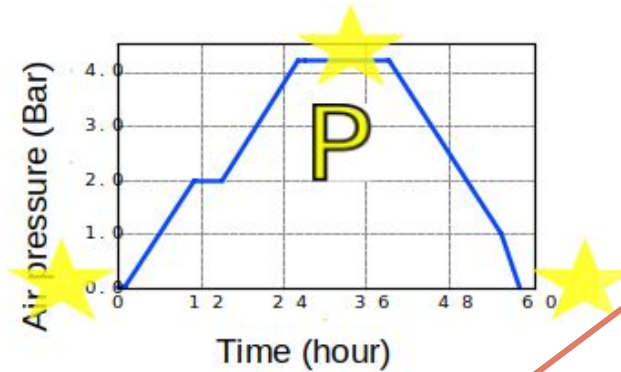
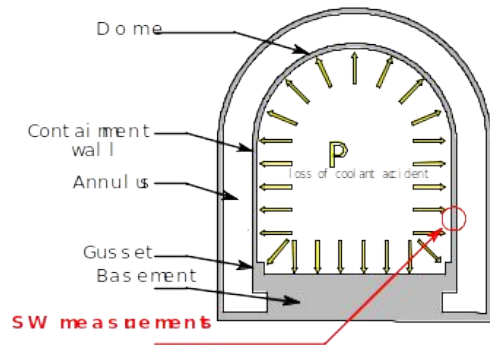
Focus on ultrasonic Surface Waves



Focus on ultrasonic Surface Waves



Focus on ultrasonic Surface Waves



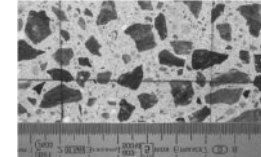
Outline

- **Recovering some concrete material properties**
 - fusion
- **Focus on Surface Waves (NDE/SHM)**
 - cover concrete
 - increasing TRL
- **Focus on Coda Waves**
 - monitoring
 - non linear
- **Fibers Optics at ultrasonics frequency**
 - project startings

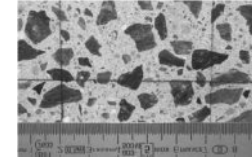
Focus on CODA Wave Interferometry

CONTEXT

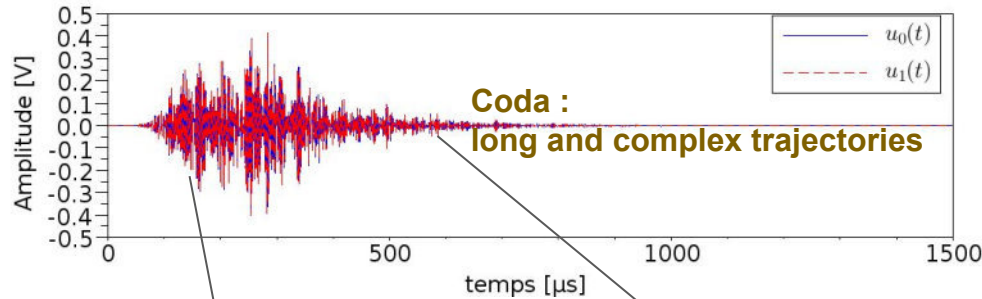
- Closed crack detection, sizing, monitoring
 - Pre-stressed concrete
 - Nuclear containment plants = ultimate barrier in the event of an accident
 - Resist internal overpressure
 - Prevent leakage
- When classical techniques fail
 - Early age detection
 - In very heterogeneous material



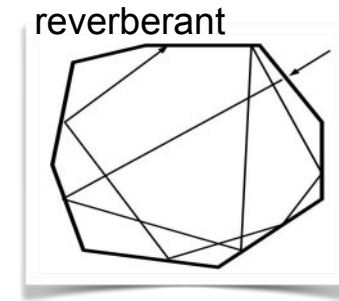
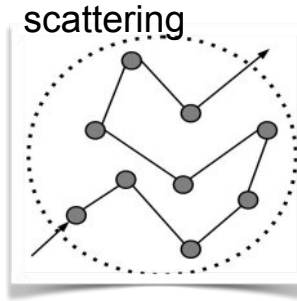
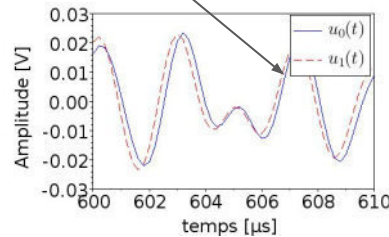
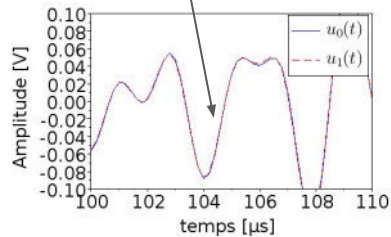
Focus on CODA Wave Interferometry



- Basic physical principle



- CWI : Stretching (state 0, state 1)



$$CC(\theta) = \frac{\int_{t_1}^{t_2} u_0[t(1+\theta)] u_1[t] dt}{\sqrt{\int_{t_1}^{t_2} u_0^2[t(1+\theta)] dt} \sqrt{\int_{t_1}^{t_2} u_1^2[t] dt}}$$

Extracted features:

$$\theta = \delta v / v$$

Velocity variation

$$Kd = 1 - CC(\theta)$$

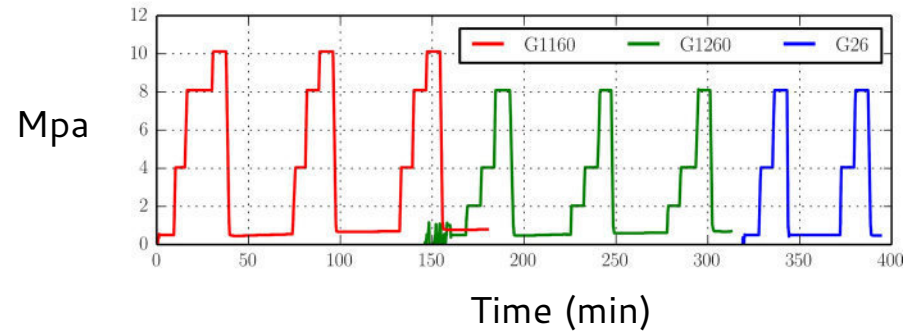
Decorrelation

R. Snieder, Coda Wave interferometry and the equilibration of energy in elastic media. *Phys. Rev. E*, 2002.

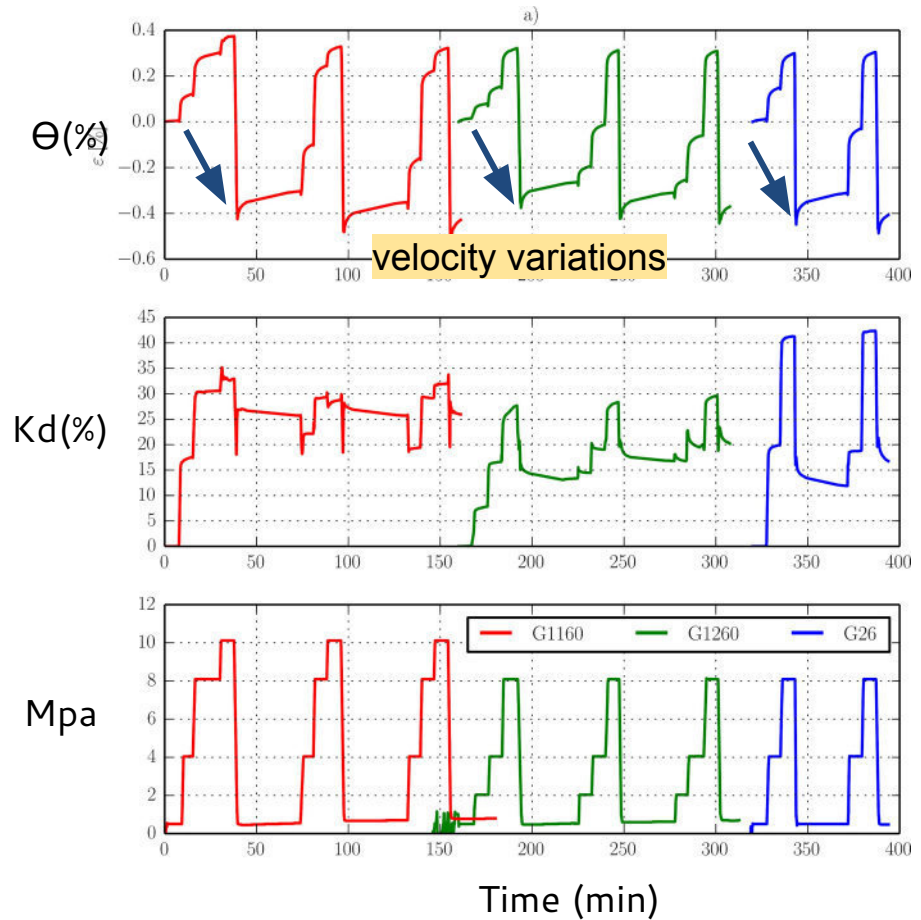
Focus on CODA Wave Interferometry



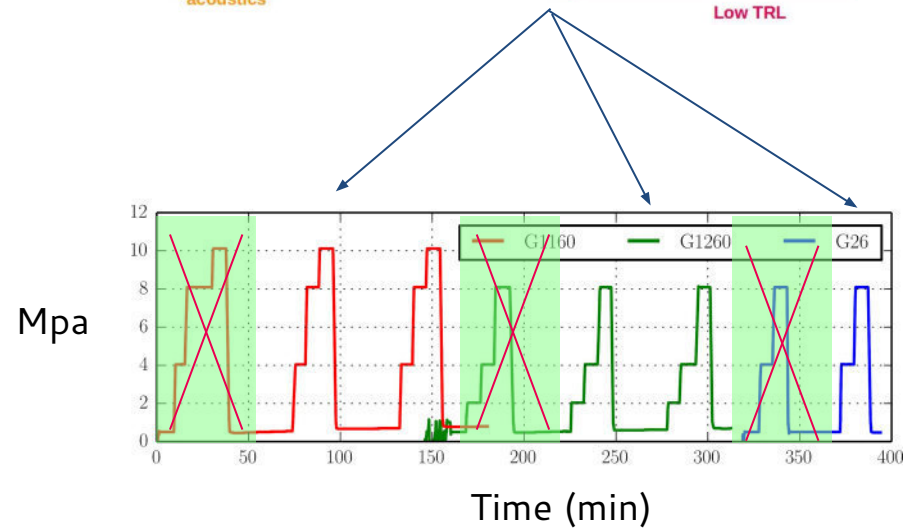
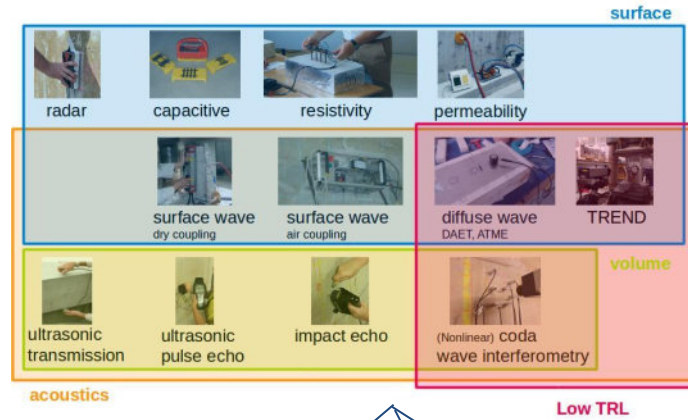
Below 30% of concrete
compressive stress



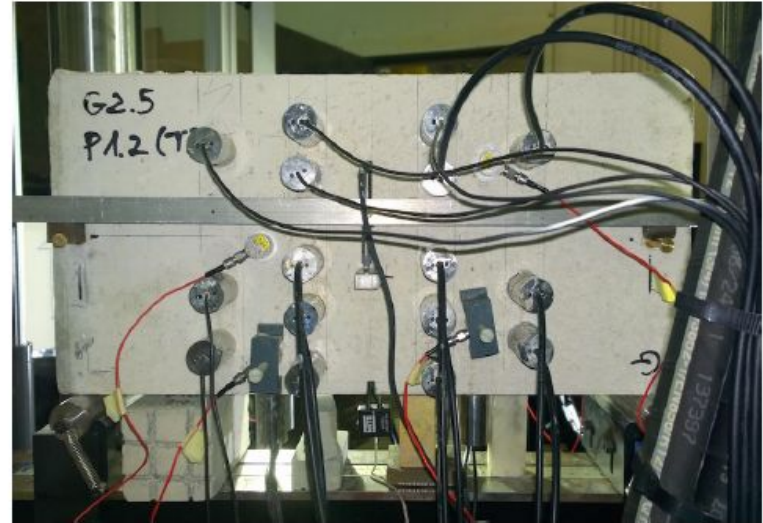
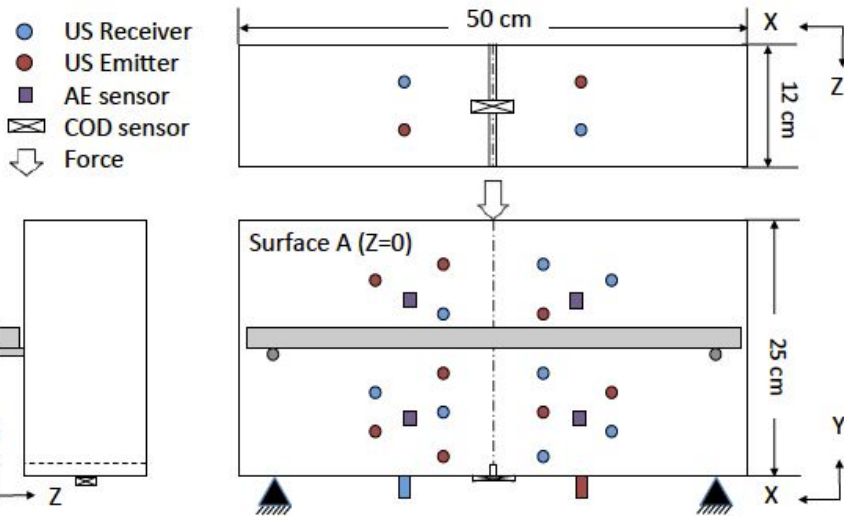
Focus on CODA Wave Interferometry



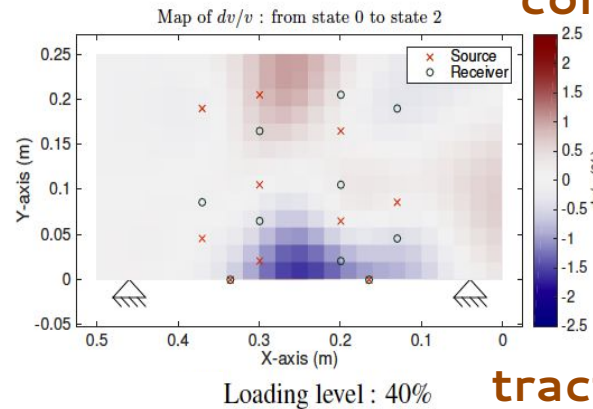
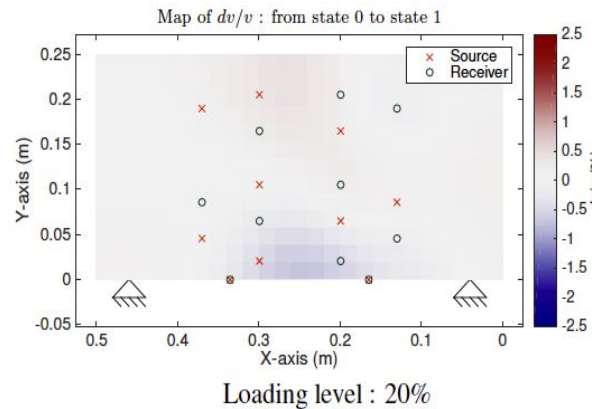
Focus on CODA Wave Interferometry



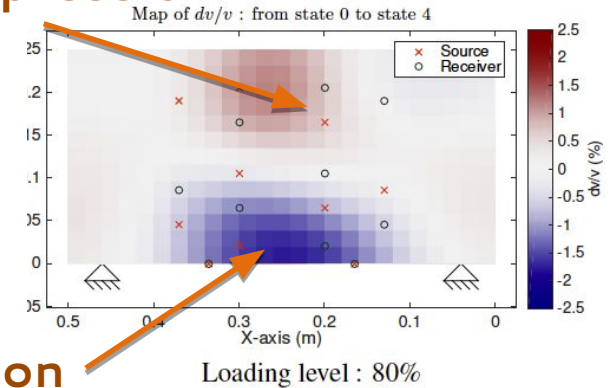
Focus on CODA Wave Interferometry



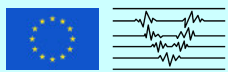
E. Larose
Y. Zhang



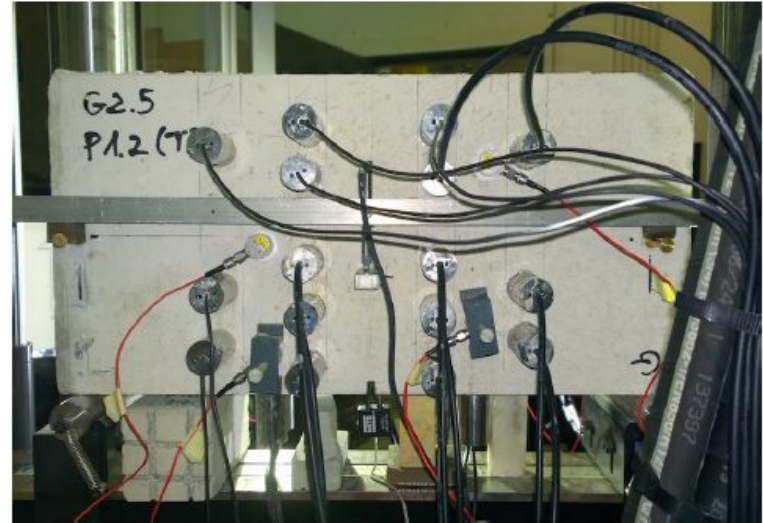
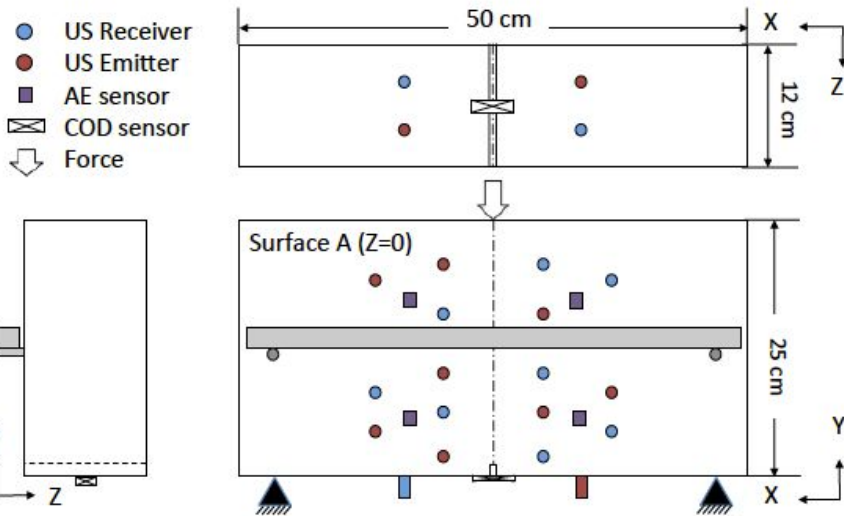
compression



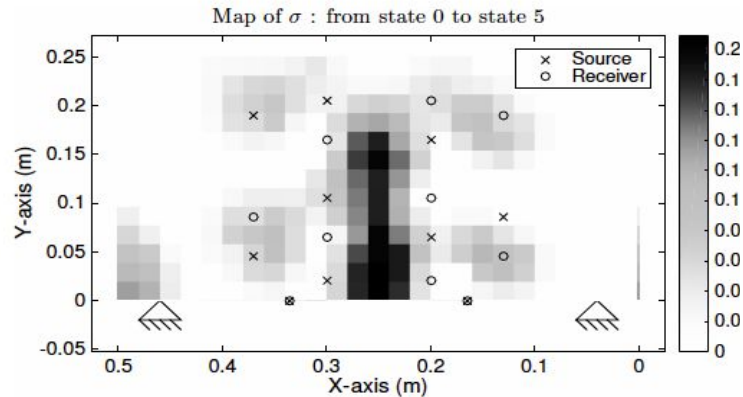
traction



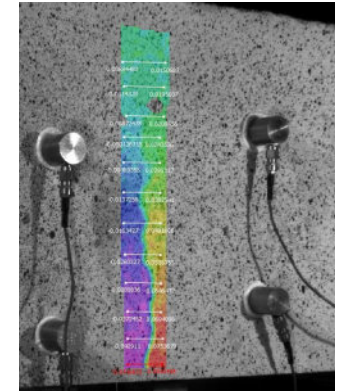
Focus on CODA Wave Interferometry



E. Larose
Y. Zhang



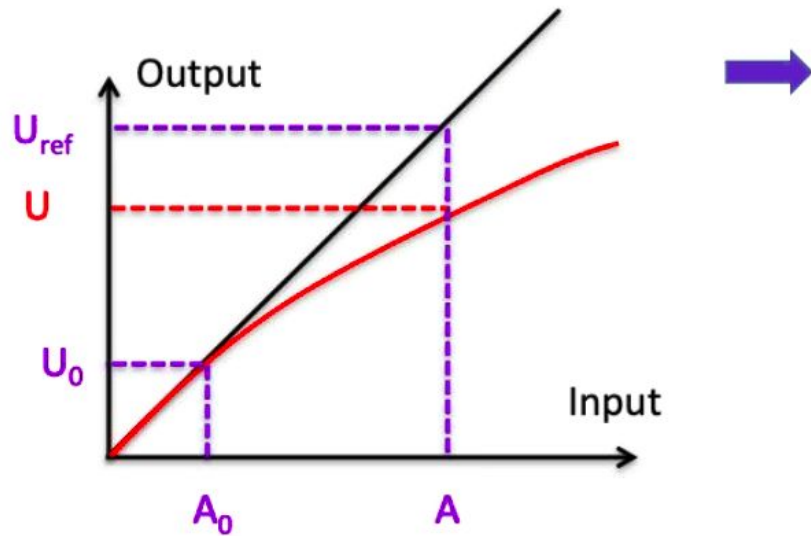
Digital Image Correlation



Focus on **Nonlinear** CODA Wave Interferometry

$$\sigma = E_0 \epsilon (1 + \beta \epsilon + \delta \epsilon^2 + \dots) + \alpha \text{Fct}(\epsilon, \text{sign}(\partial \epsilon / \partial t))$$

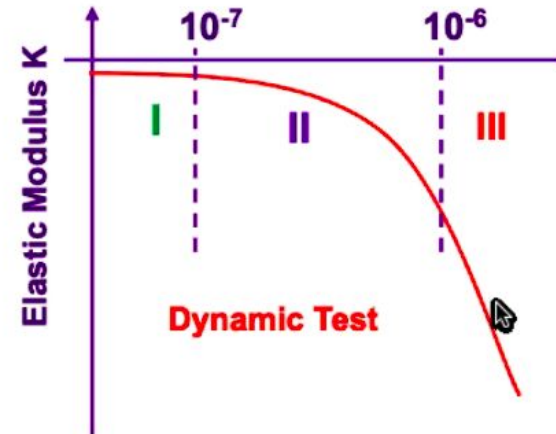
Zone I Zone II Zone III



Linear Elasticity

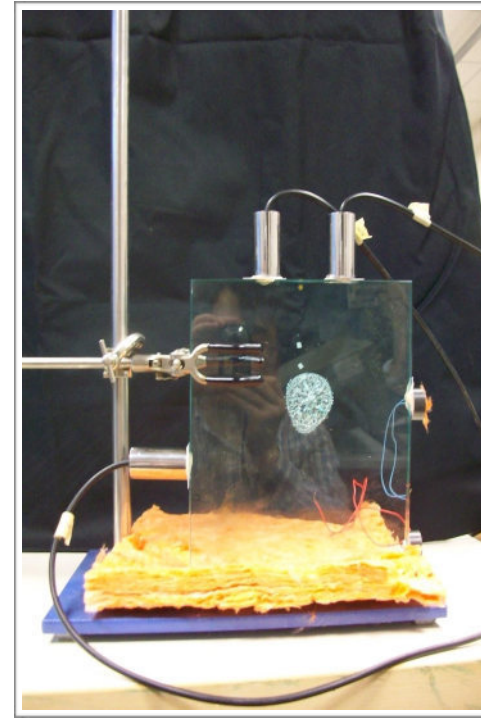
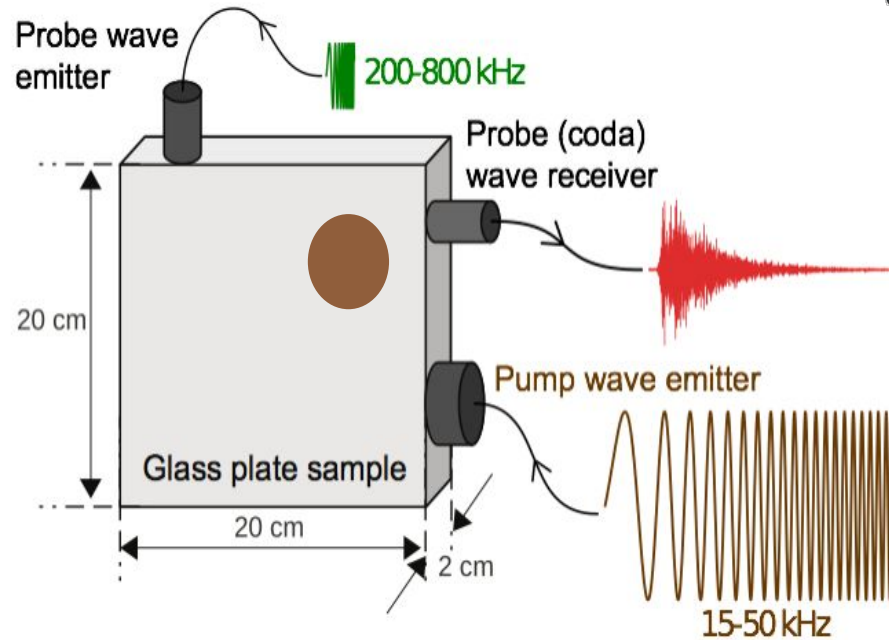
Quadratic or Cubic elasticity (Classical nonlinearity)

Hysteretic nonlinear behaviour



Focus on **Nonlinear** CODA Wave Interferometry

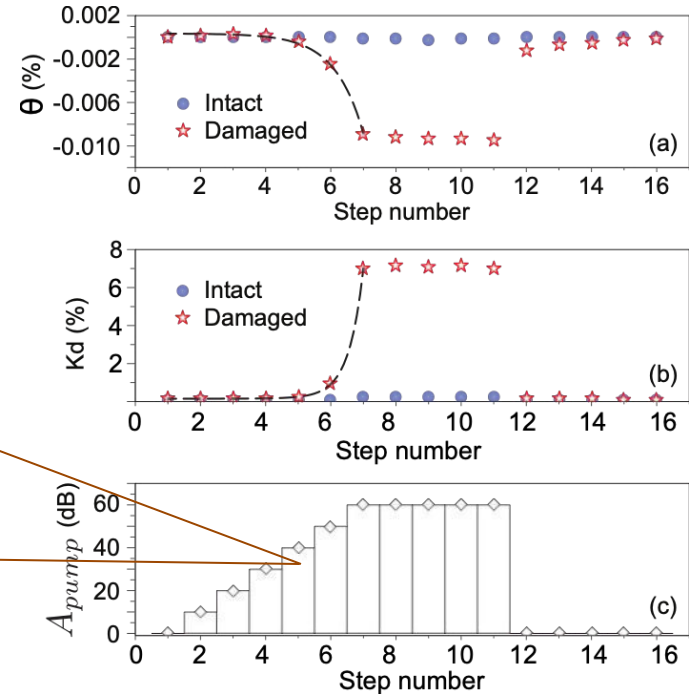
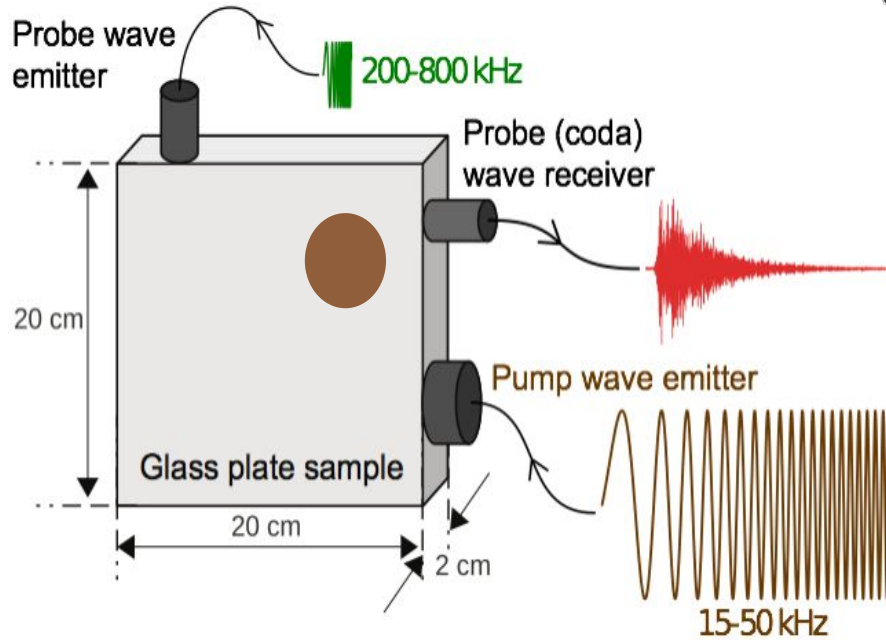
$$\sigma = E_0 \epsilon (1 + \beta \epsilon + \delta \epsilon^2 + \dots) + \alpha \text{Fct}(\epsilon, \text{sign}(\partial \epsilon / \partial t))$$



Zhang et al, Nonlinear mixing of ultrasonic coda waves with lower frequency-swept pump waves for a global detection of defects in multiple scattering media. *Journal of Applied Physics*, 2013.

Focus on **Nonlinear** CODA Wave Interferometry

$$\sigma = E_0 \epsilon (1 + \beta \epsilon + \delta \epsilon^2 + \dots) + \alpha \text{Fct}(\epsilon, \text{sign}(\partial \epsilon / \partial t))$$



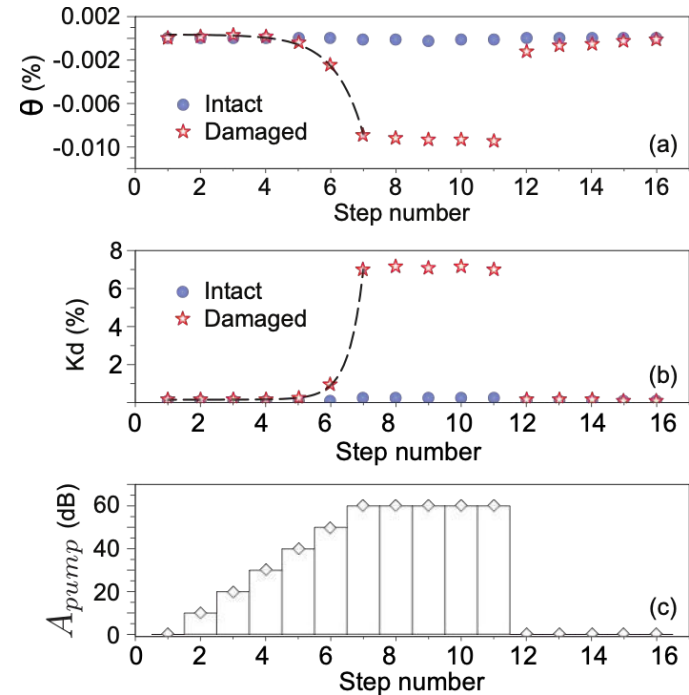
Zhang et al, Nonlinear mixing of ultrasonic coda waves with lower frequency-swept pump waves for a global detection of defects in multiple scattering media. *Journal of Applied Physics*, 2013.

Focus on **Nonlinear** CODA Wave Interferometry

$$\sigma = E_0 \epsilon (1 + \beta \epsilon + \delta \epsilon^2 + \dots) + \alpha \text{Fct}(\epsilon, \text{sign}(\partial \epsilon / \partial t))$$

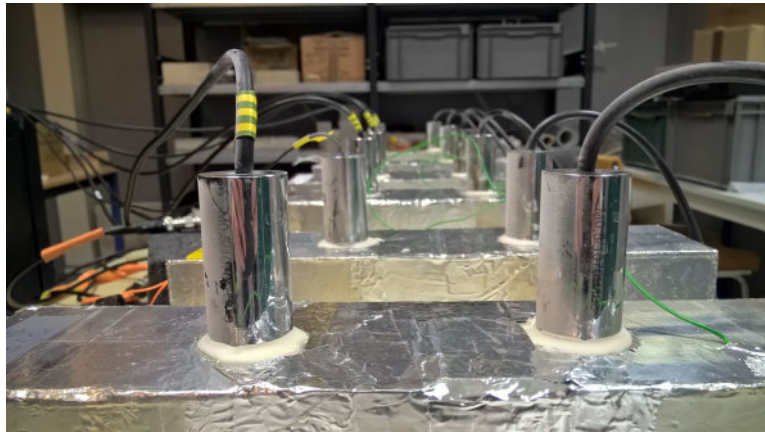
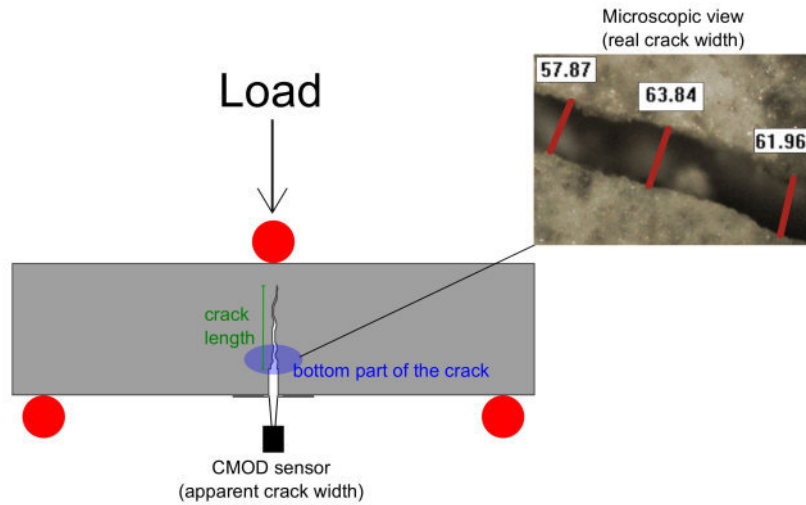
$$\theta \propto \alpha_{\theta} (A_{\text{pump}})$$

$$Kd \propto \alpha_{Kd} (A_{\text{pump}})^2$$

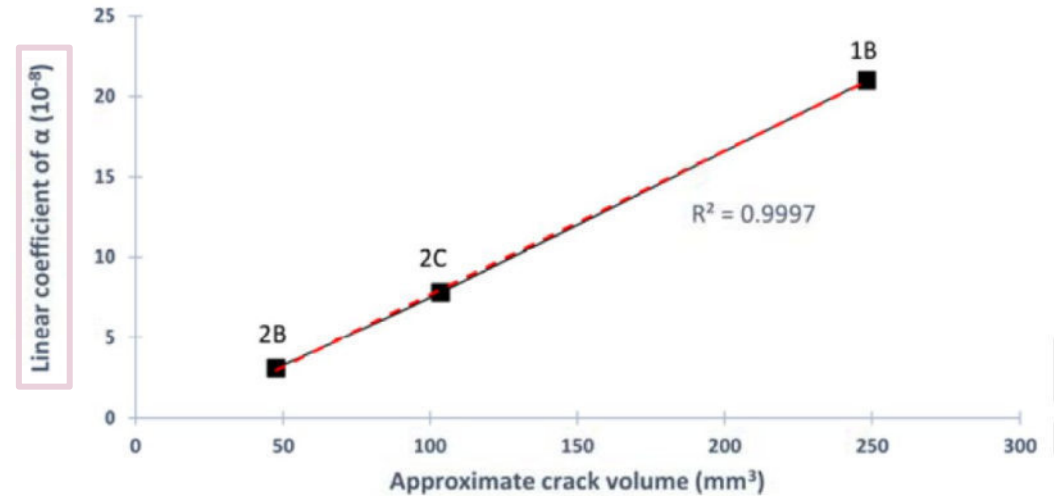


Zhang et al, Nonlinear mixing of ultrasonic coda waves with lower frequency-swept pump waves for a global detection of defects in multiple scattering media. *Journal of Applied Physics*, 2013.

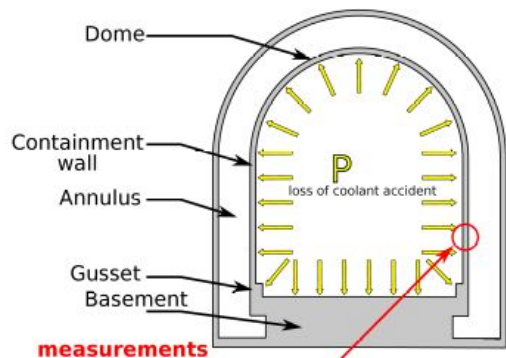
Focus on **Nonlinear** CODA Wave Interferometry (NCWI)



$$\theta \propto \alpha_{\theta}(A_{pump})$$

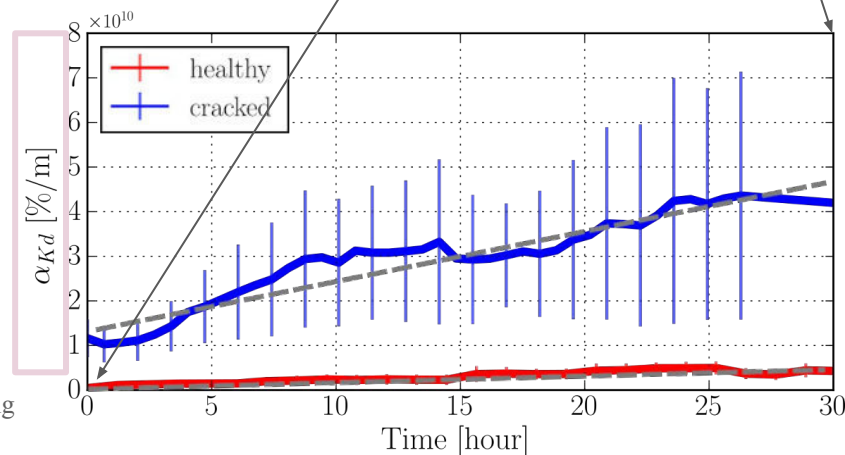
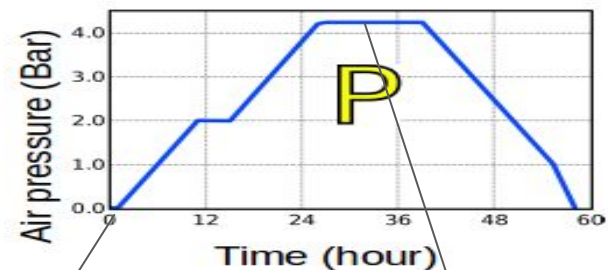


Focus on **Nonlinear** CODA Wave Interferometry (NCWI)

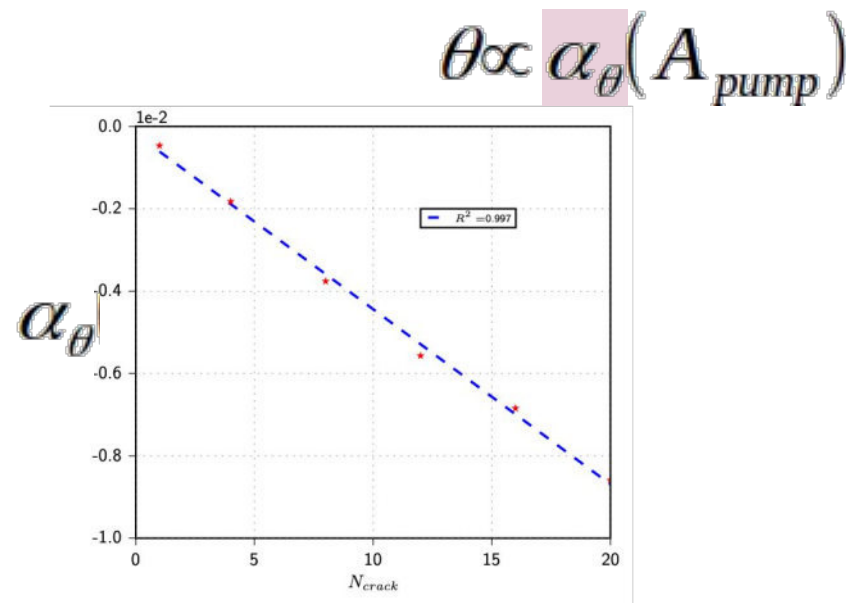
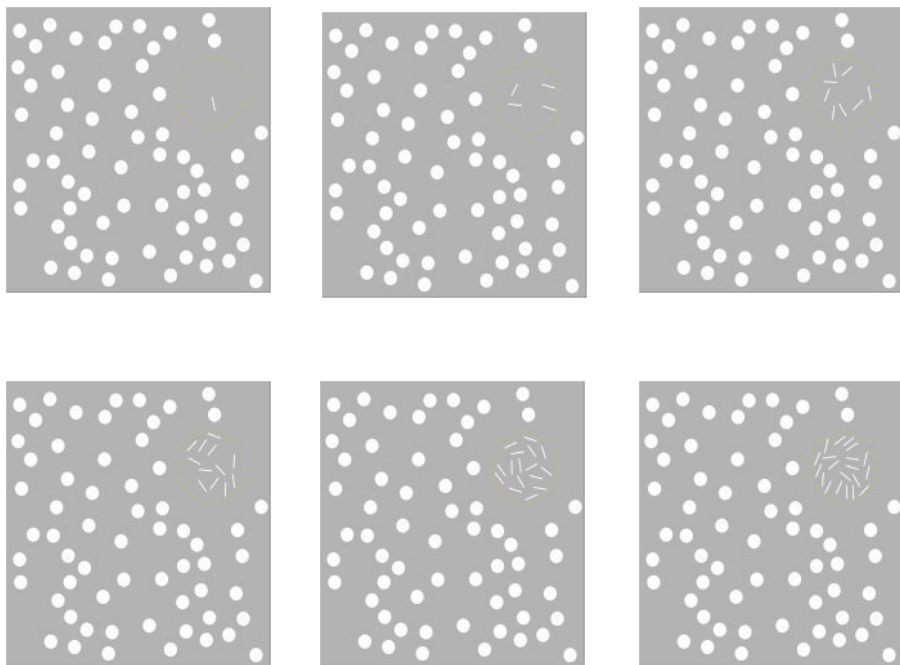


Legland J.-B. et al, Evaluation of crack status in a meter-size concrete structure using the ultrasonic nonlinear coda wave interferometry. *JASA*, 2017

$$Kd \propto \alpha_{Kd} (A_{pump})^2$$



Focus on **Nonlinear** CODA Wave Interferometry (NCWI)

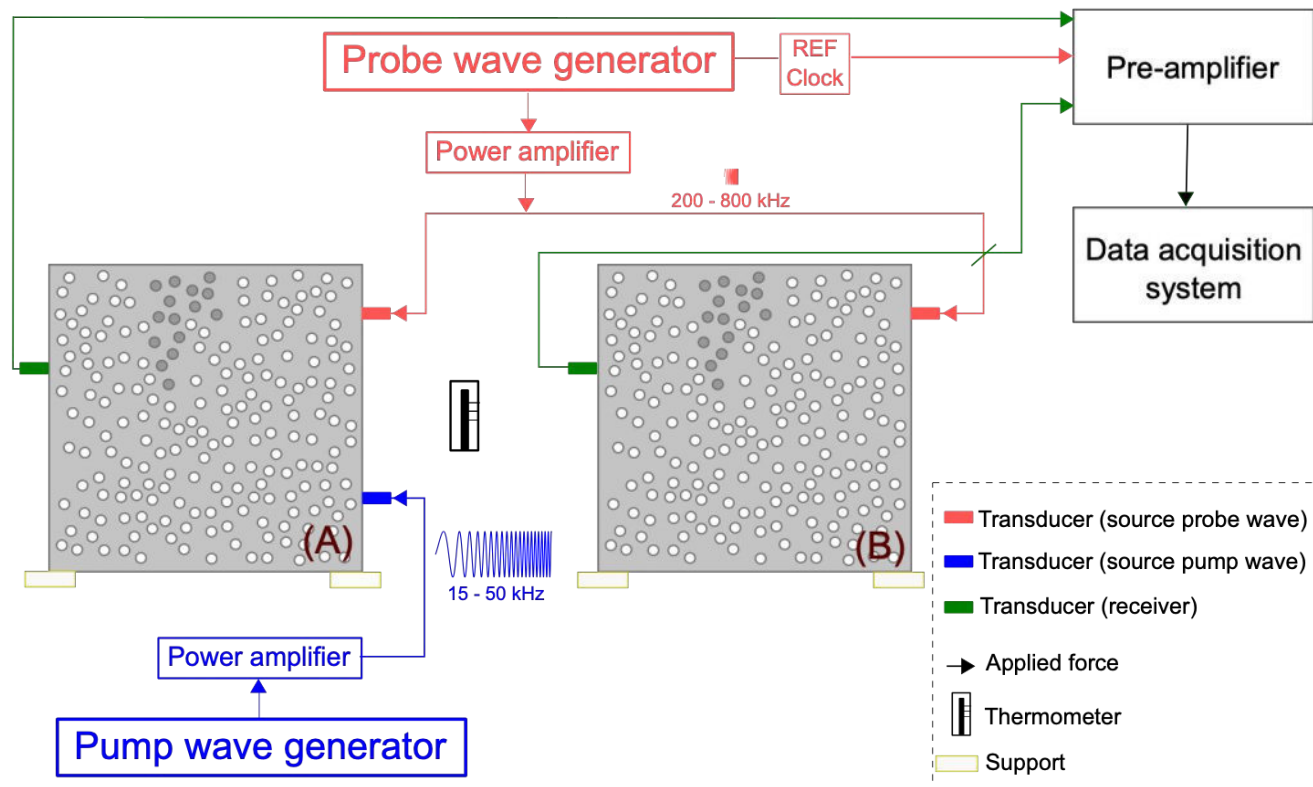
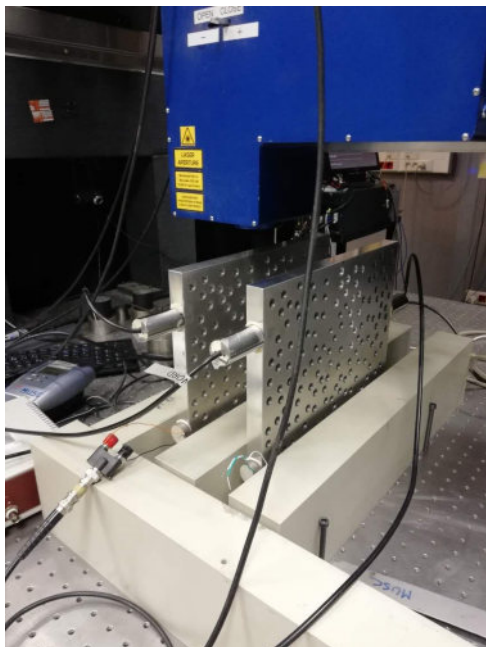


$$\theta = \alpha_{\theta}^{\sum L} \times \left(\sum \frac{\Delta L_{crack}}{L_{crack}} \right)$$

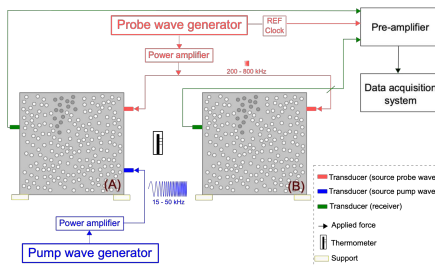
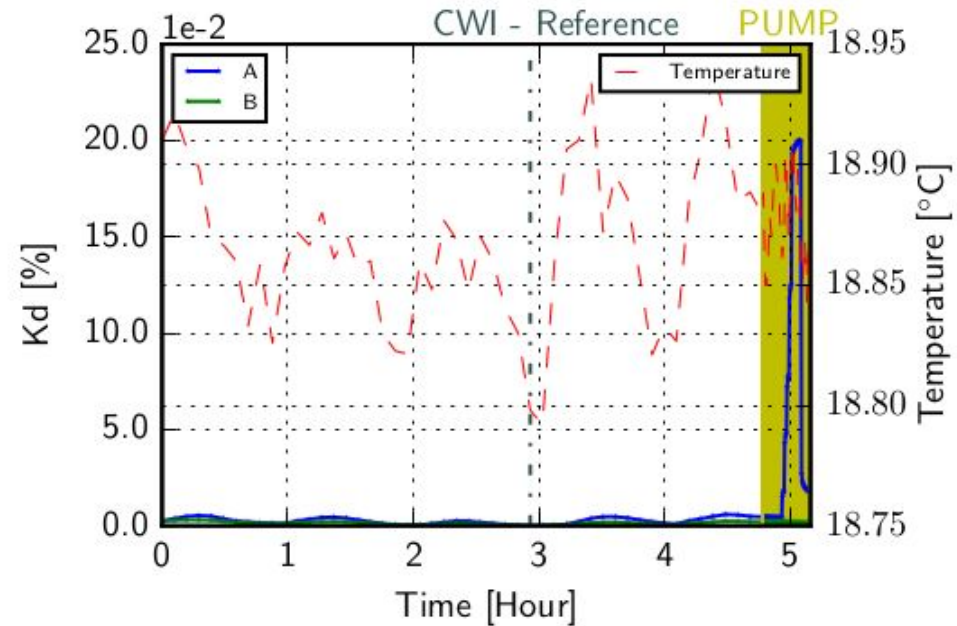
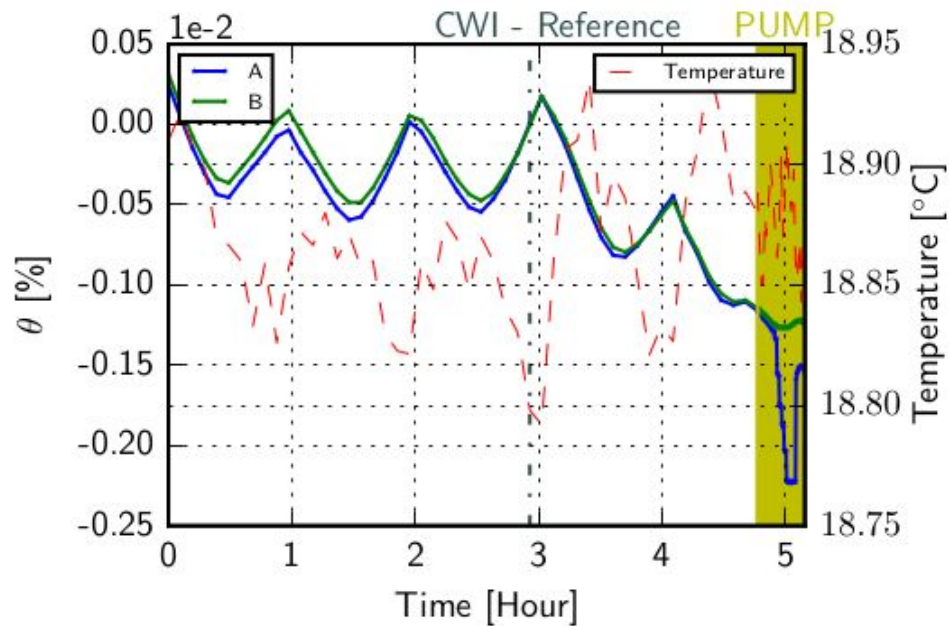
$$Kd = \alpha_{Kd}^{\sum L} \times \left(\sum \frac{\Delta L_{crack}}{L_{crack}} \right)^2$$

G. Chen et al. Numerical modeling of ultrasonic coda wave interferometry in a multiple scattering medium with a localized nonlinear defect, *Wave Motion*, 2017

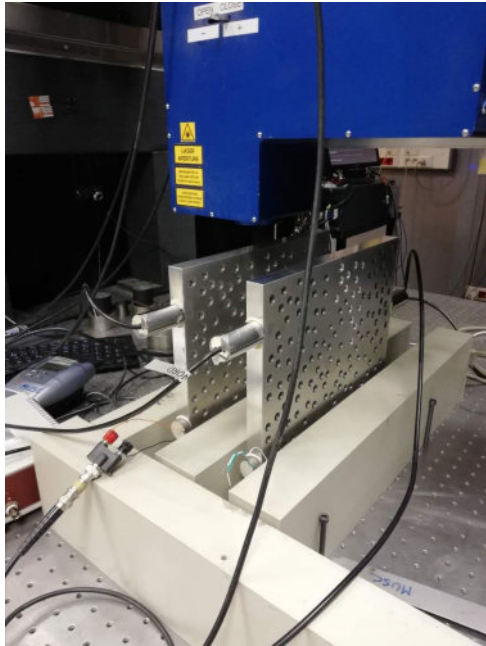
Focus on **Nonlinear** CODA Wave Interferometry (NCWI)



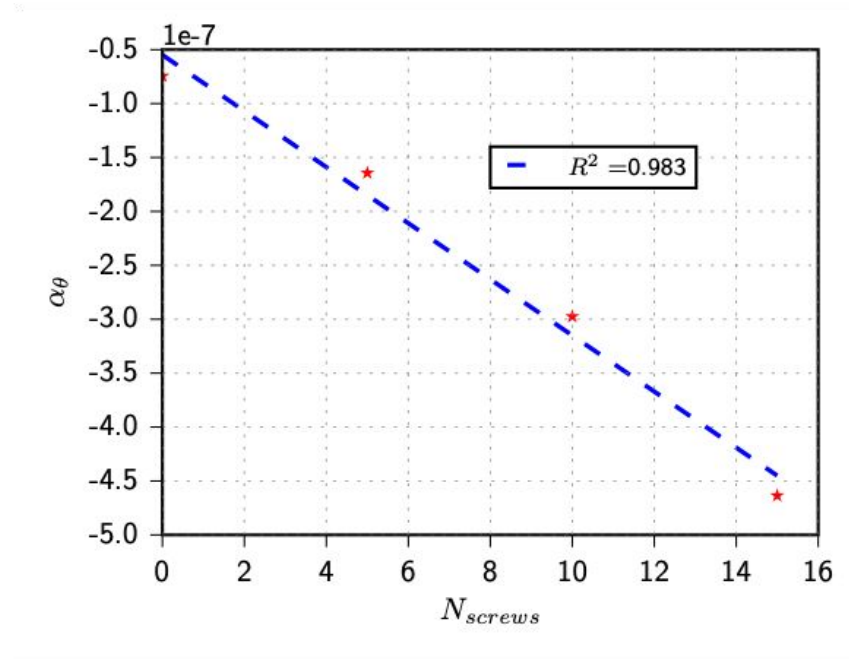
Focus on **Nonlinear** CODA Wave Interferometry (NCWI)



Focus on **Nonlinear** CODA Wave Interferometry (NCWI)



$$\theta = \alpha_{\theta} \sum L \times (\Delta L \times N) = \alpha_{\theta} \sum L \times (\sum \Delta L)$$

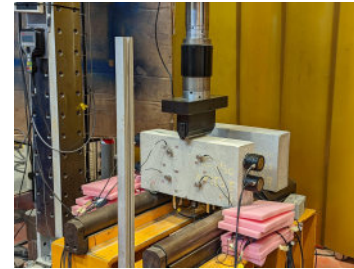
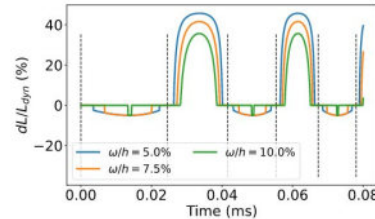
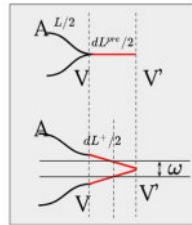
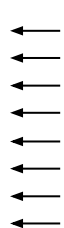
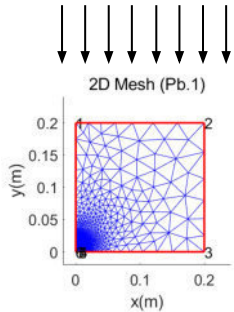


Focus on **Nonlinear** CODA Wave Interferometry (NCWI)

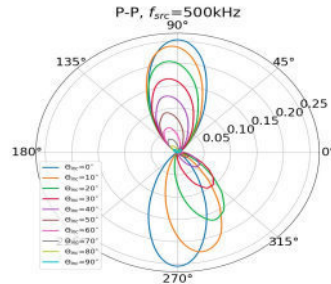
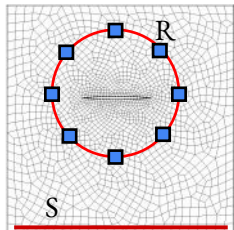
Ongoing work: imagery of closed cracks (without a reference to a "sound" material)

- A forward model with "few" parameters that can quantify the effect of the pump on the crack (maximum amplitude of the pump at one level, Young's Modulus, Poisson's ratio, crack length L , crack eighth, crack pre-closure length dL^{pre} , opening threshold ω)

Statique FEM

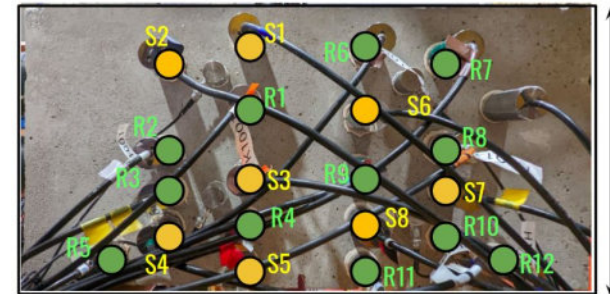


Dynamic SEM2D



average scattering cross section for a given maximum amplitude of the pump at one level

(P-P, P-S, S-S, S-P)



250 mm



500 mm

Outline

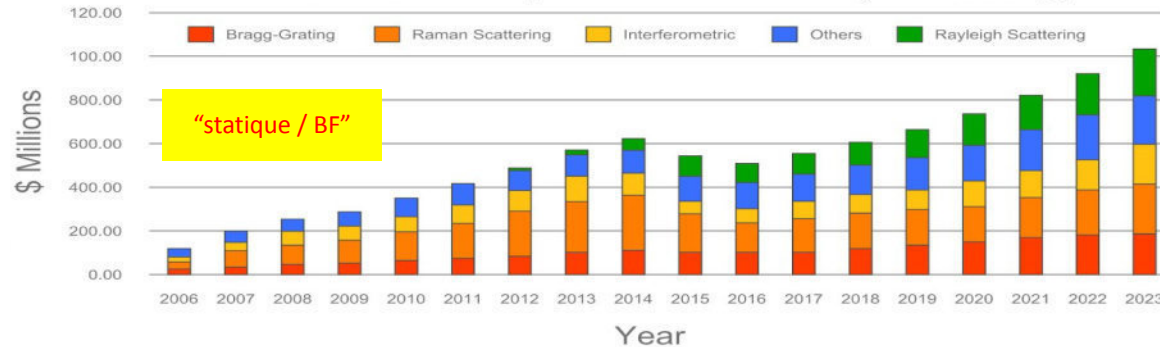
- **Recovering some concrete material properties**
 - fusion
- **Focus on Surface Waves (NDE/SHM)**
 - cover concrete
 - increasing TRL
- **Focus on Coda Waves**
 - monitoring
 - non linear
- **Fibers Optics at ultrasonics frequency**
 - project startings

Fiber Optics at ultrasonic frequency

CONTEXT

- Long term ultrasonic monitoring of concrete
 - Sensor durability in harsh environment (salty, radioactive, high temperature, ...)
 - Limited footprint of Fiber Optic
 - + Several localized sensing points along a single cable
 - Broadband transducer

Distributed Fiber Optic Sensor Market by Technology



Bado & Casas, A Review of Recent Distributed Optical Fiber Sensors Applications for Civil Engineering Structural Health Monitoring, 2021, Sensors, 21(5), 1818. [doi](#)
Liu *et al.*, Distributed Fiber-Optic Sensors for Vibration Detection, 2016, Sensors, 16(8). [doi](#)

Fiber Optics at ultrasonic frequency

- **Technologies** : DAS, OFDR (Rayleigh, Bragg), FBG (TDM, WDM, reflectometry,...)
- **Industrials** : optics11 (NL, pastille), ibsen photonics (Dk), redondo (USA), Ifos (USA), SmartFibers (USA), Micron-Optics (Luna, USA)... <~20kHz
- **Academics** : Virginia Tech, CEA, Allemagne (BAM, Univ. Munich, IPHT...), UK (Univ. Southampton), Hong-Kong Polythec Univ....
- **FBGs** in development for ultrasonics on steel and composite structures

ANR-21-CE04-0007 FO-US AIMS

- increase frequency (sampling at several MHz)
- increase number of measurement points (at least 32)
- long distances
- reasonable cost

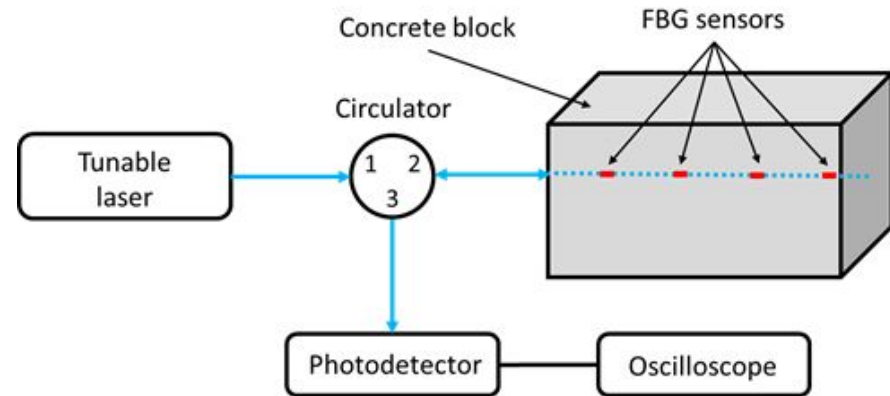
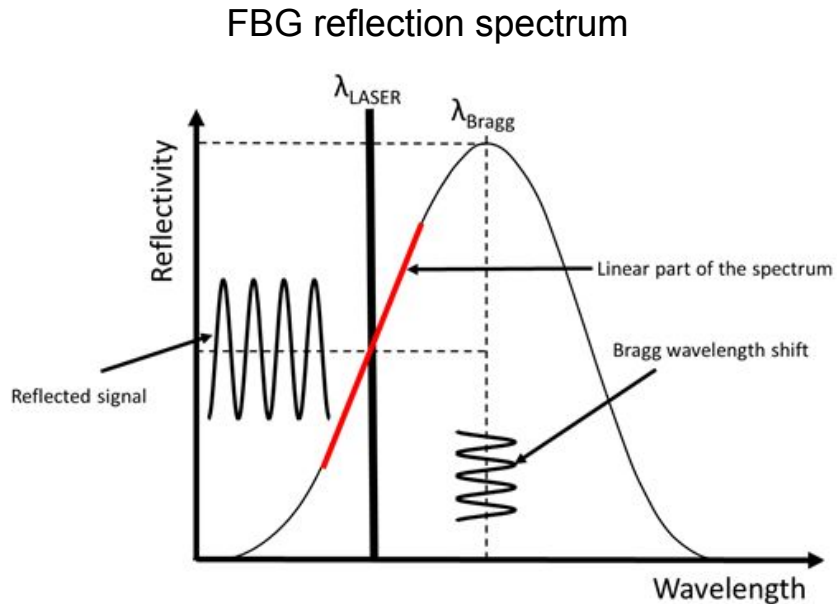


Fiber Optics at ultrasonic frequency

FIBER BRAGG GRATING (FBG) PRINCIPLE



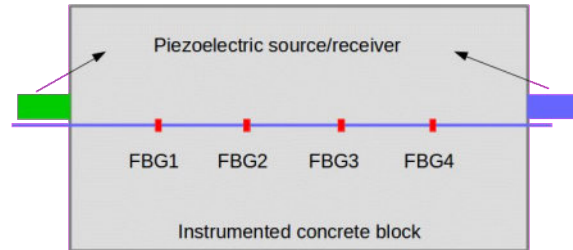
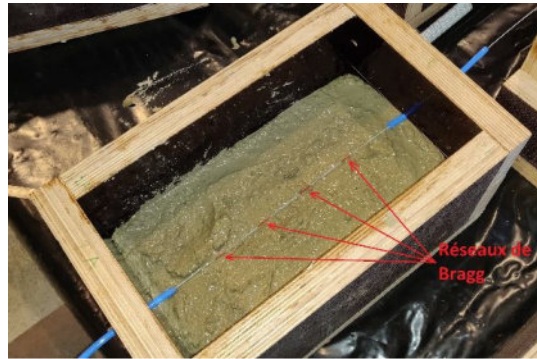
- Tunable laser source
- FGB interrogator system
- Edge filtering method



T. Druet, B. Chapuis, M. Jules, G. Laffont, E. Moulin. 2018. "Passive guided waves measurements using fiber Bragg gratings sensors", *The Journal of the Acoustical Society of America* 144, 1198.

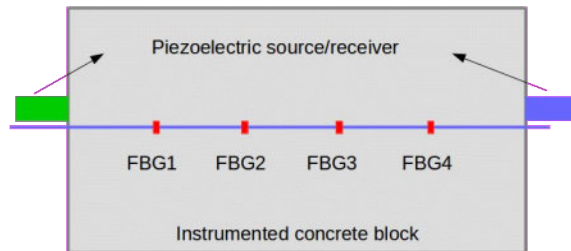
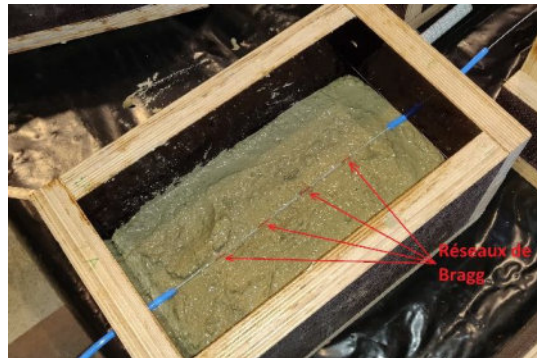
Fiber Optics at ultrasonic frequency

- 16 cm x 16 cm x 30 cm concrete blocks
 - $R_c = 18.8 \text{ MPa} \pm 3.5 \text{ MPa}$
- Glued piezoelectric transducers

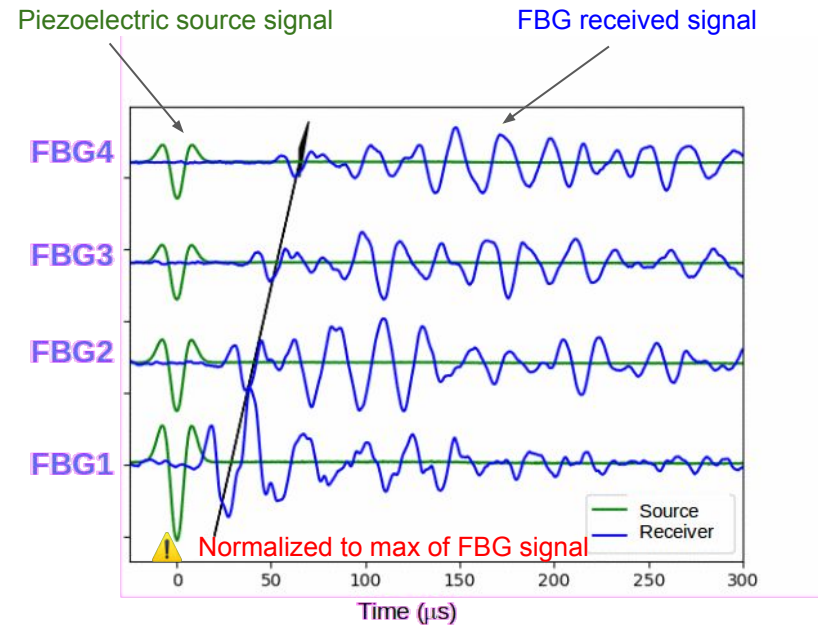


Fiber Optics at ultrasonic frequency

- 16 cm x 16 cm x 30 cm concrete blocks
 - $R_c = 18.8 \text{ MPa} \pm 3.5 \text{ MPa}$

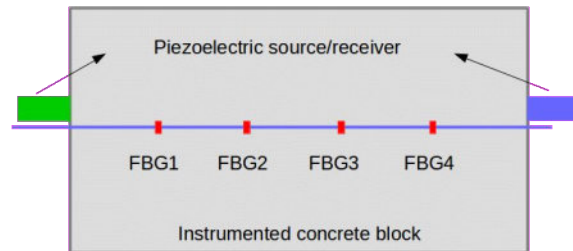
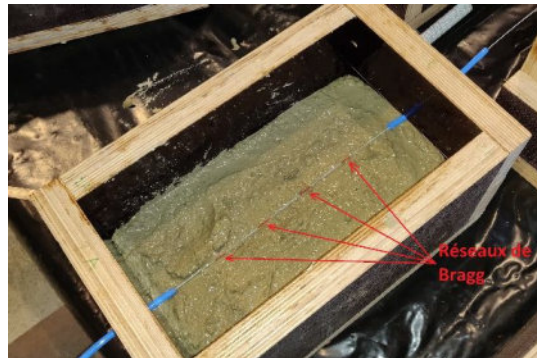


- Glued piezoelectric transducers
 - Source : 54kHz



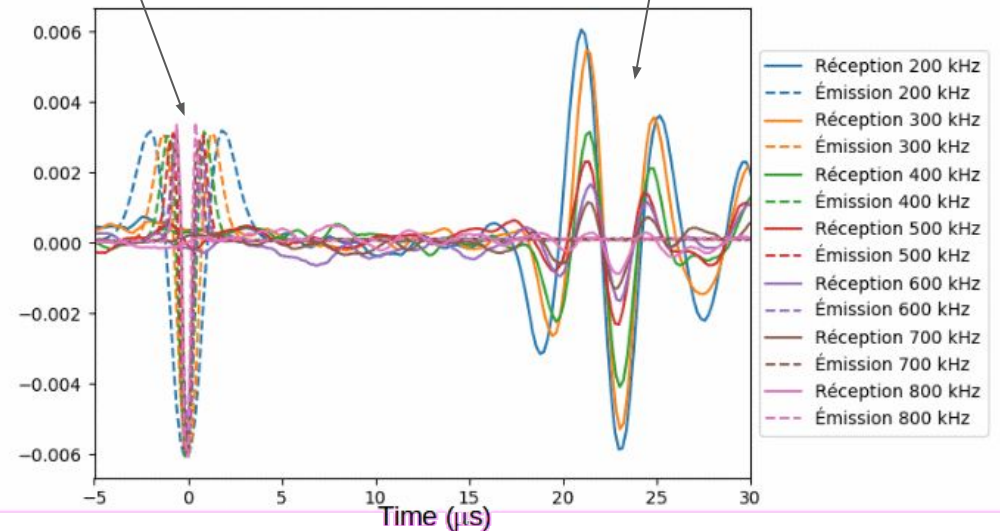
Fiber Optics at ultrasonic frequency

- 16 cm x 16 cm x 30 cm concrete blocks
 - $R_c = 18.8 \text{ MPa} \pm 3.5 \text{ MPa}$

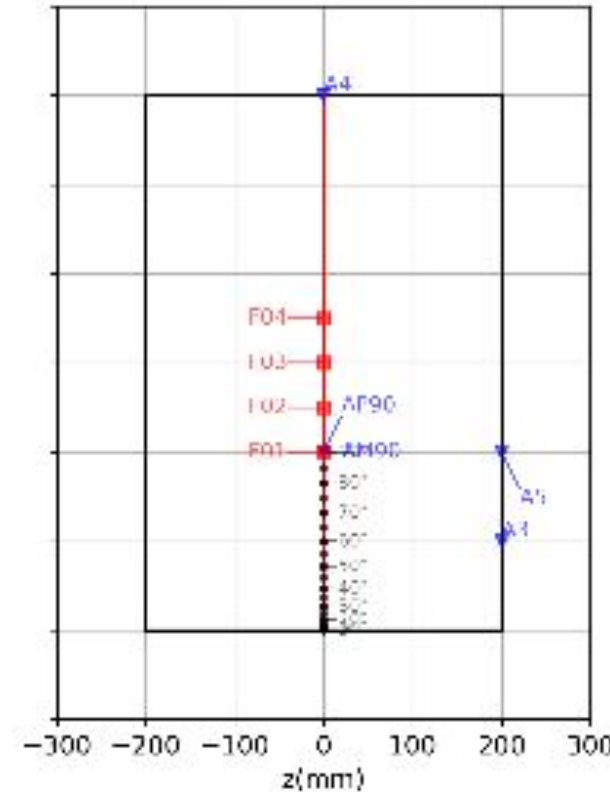
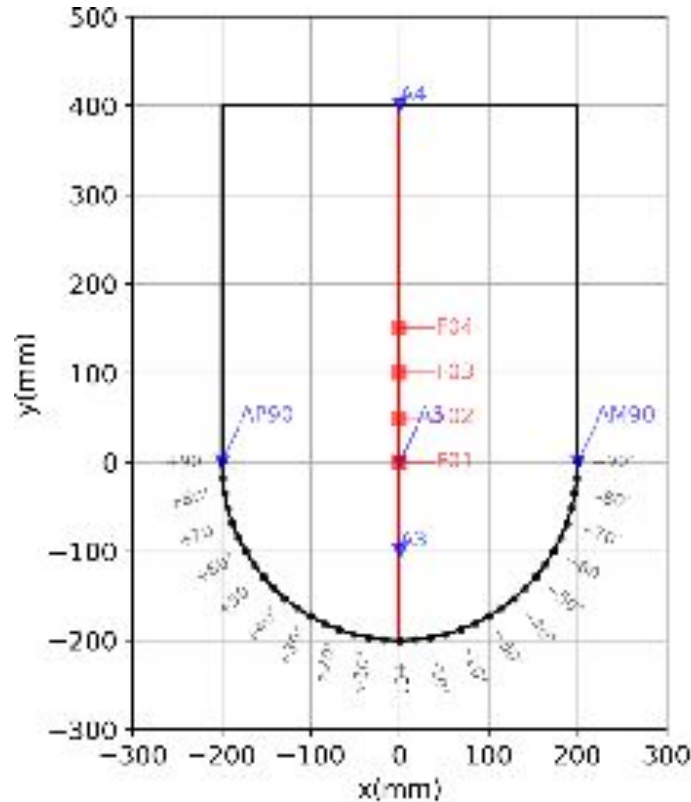


- Glued piezoelectric transducers
 - Source : 200kHz-800kHz

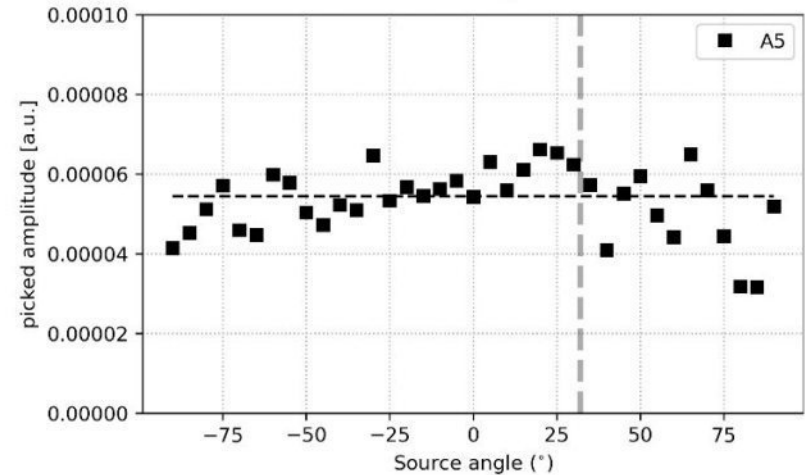
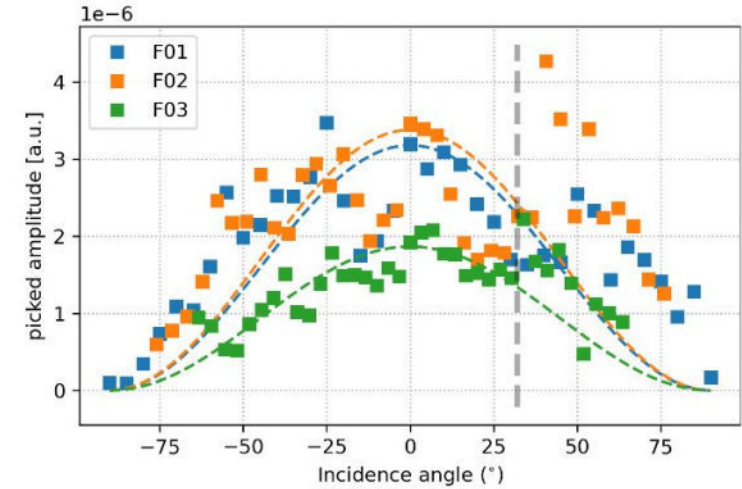
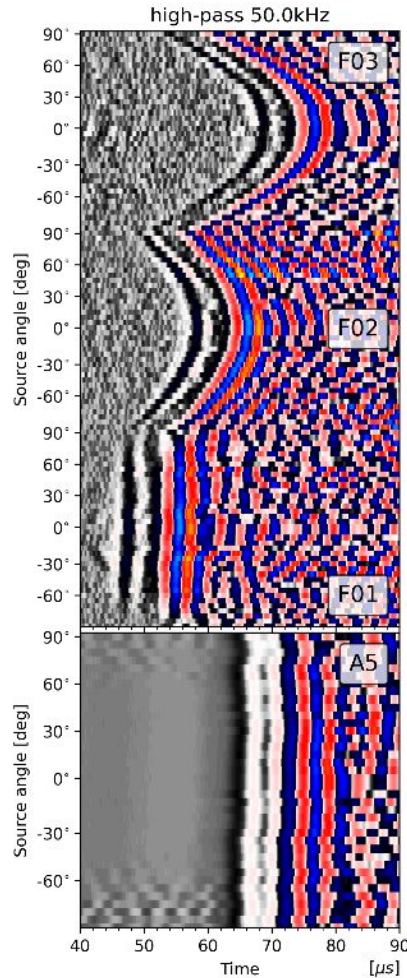
Piezoelectric source signal FBG1 received signal



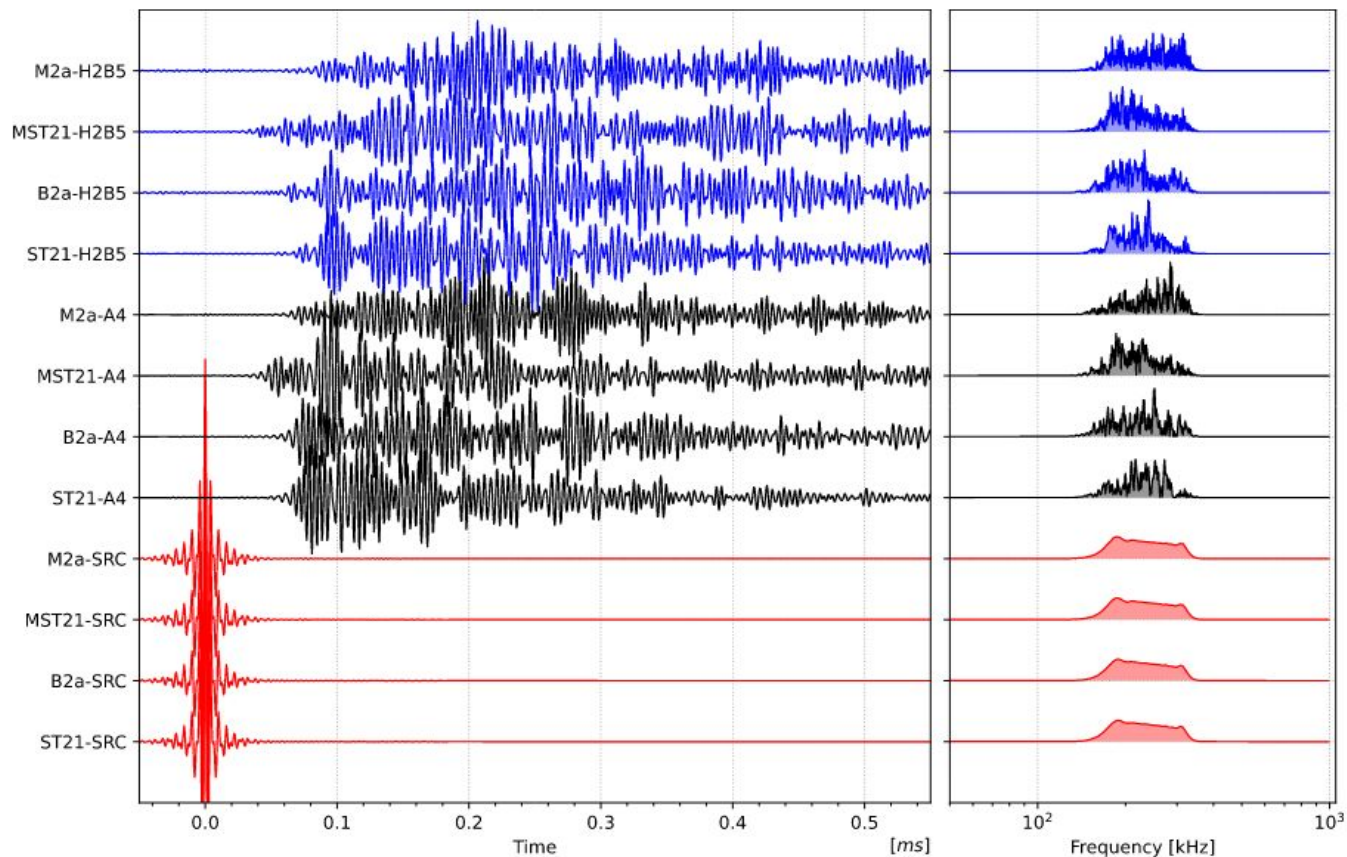
Fiber Optics at ultrasonic frequency



Fiber Optics at ultrasonic frequency

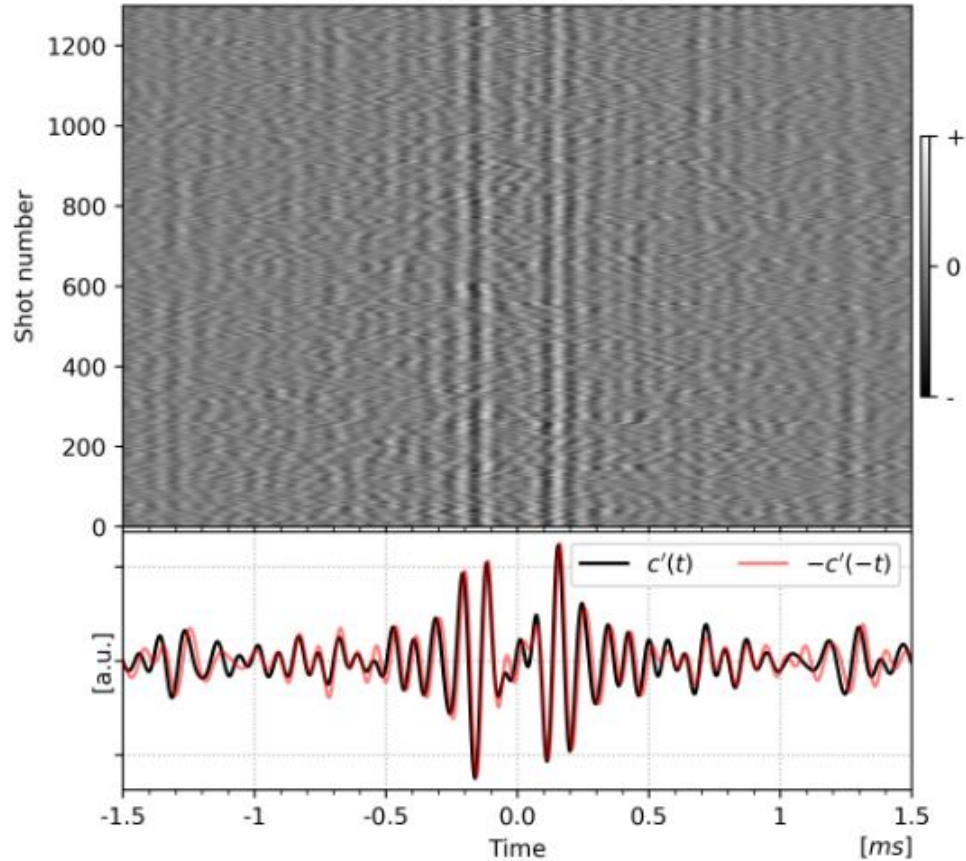


Fiber Optics at ultrasonic frequency

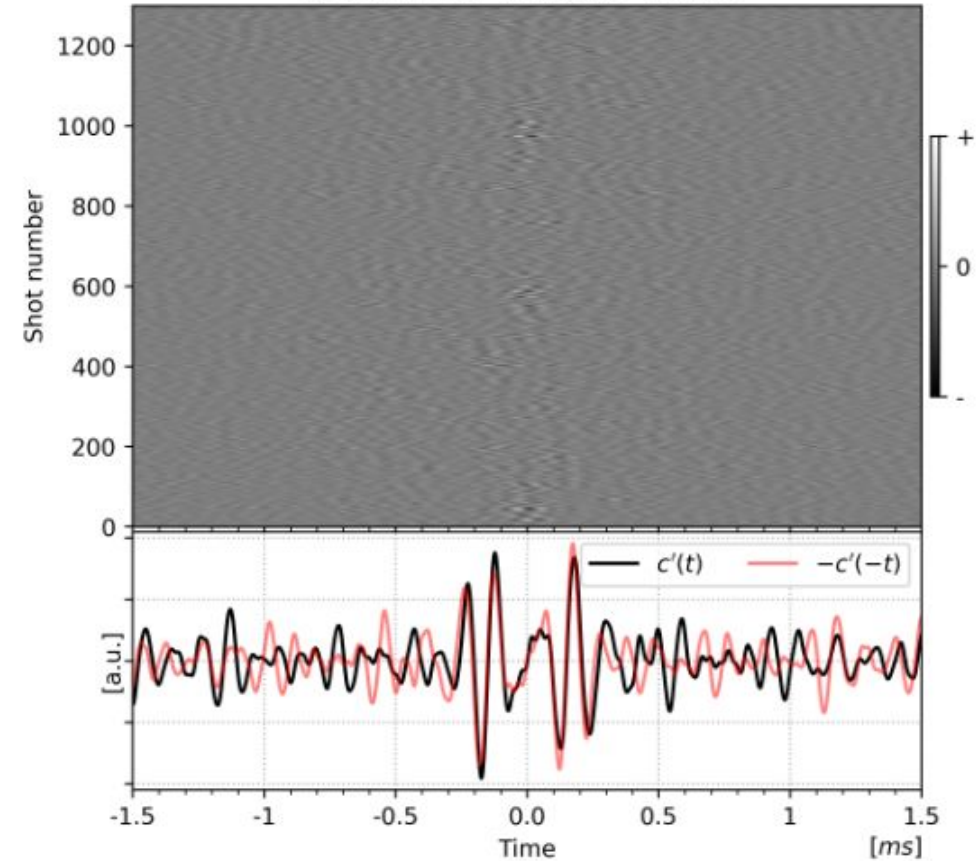


Fiber Optics at ultrasonic frequency

[200], A4 - A5, 5 - 15 kHz

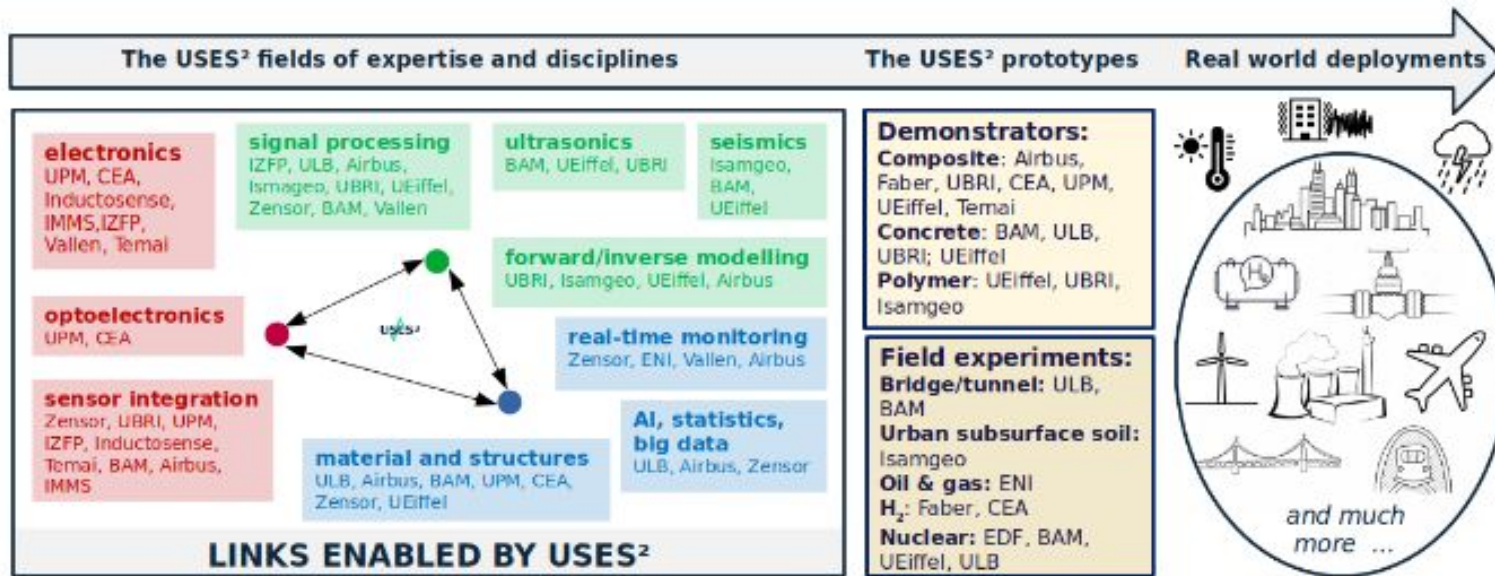


[200], H2B3 - H2B5, 5 - 15 kHz





USES of novel UltraSonic and Seismic Embedded Sensors for the non-destructive evaluation and structural health monitoring of infrastructure and human-built objects





Coda waves, Surface Waves, Fiber Optics... Some challenges and results about the monitoring of concrete structures with ultrasonic waves

Odile Abraham



LABORATOIRE GEOEND
GÉOPHYSIQUE ET
ÉVALUATION NON
DESTRUCTIVE